

# ARIES-DB Design Issues

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- TBR-related issues – what's new?
- ITER reweldability limits for 316-SS – an update.
- OB DCLL blanket segmentation – a suggestion.
- Degradation of physical properties with neutron irradiation – few examples.



# TBR-Related Issues

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## What's new?

- T cost to supply 1% deficiency in breeding.
- New experimental results measuring LiPb tritium production rate (TPR).
- Impact of “plasma burn-up fraction” on TBR requirements.
- Net TBR comparison: ARIES vs UCLA.
- Li content in LiPb eutectic. **17 at%** or **15.7 at%**?



# T cost to Supply 1% Deficiency in Breeding

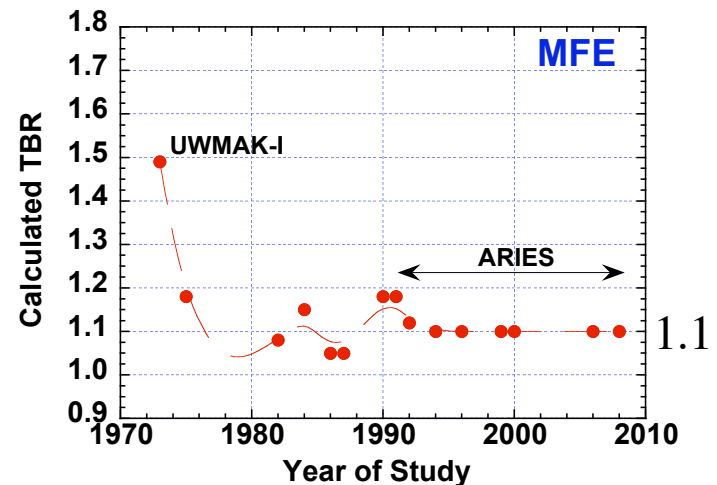
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- **T cost is excessive:**
  - \$30,000 / g of T - Canada
  - > \$30,000 / g of T - US (including shipping/handling)
- 1% less breeding  $\Rightarrow$  Shortage of  $\sim 1$  kg of T/y\* for 2 GW  $P_f$
- Cost of purchasing T exceeds \$100,000/day.

Calculated TBR should be accurately estimated  
to avoid purchasing T during operation

\* Based on 55.6 kg/y per GW  $P_f$ .

# TBR Requirements



- **Background info:**

- **ARIES** designs considered Calculated TBR of 1.1 for liquid breeders
- Breeding margin (TBR -1) divided into 4 categories:
  - Margin for known deficiencies in nuclear data (6\*-10%)
  - Margin for known deficiencies in modeling (3\*-7%)
  - Margin for unknown uncertainties in design elements (0\*-3%)
  - Margin for T bred in excess of T consumed in plasma (1\*-2%).

- **New evaluation/assessment:**

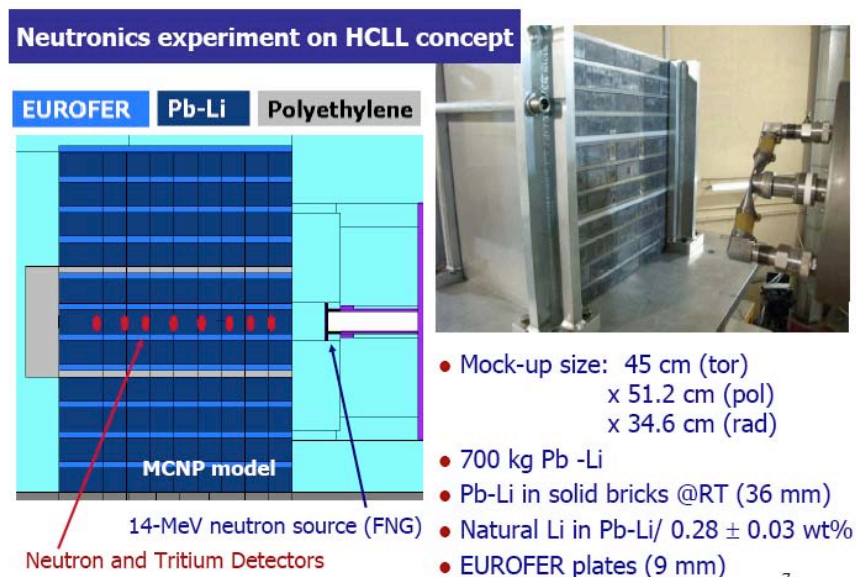
- FNG experimental measurement of LiPb tritium production rate (Margin # 1)
- Sensitivity of “excess T bred” to “plasma burn-up fraction” (Margin # 4).

\* Considered for ARIES LiPb designs.

# FNG Experiment @ ENEA Italy

B. Batistoni et al., “Neutronics Experiments on HCPB and HCLL TBM Mock-ups in Preparation of Nuclear Measurements in ITER,”

Presented at ISFNT-9, Oct. 11-16, 2009, Dalian, China.



Calculations correctly estimate TPR within total experimental uncertainty (~7% - too large). Future experiments will reduce uncertainties in:

- Experimental results
- Measurement of Li content in LiPb.

These results suggest reducing TBR margin for nuclear data deficiencies from 6% to 3% until FNG conducts new LiPb experiments with more accurate measurements.

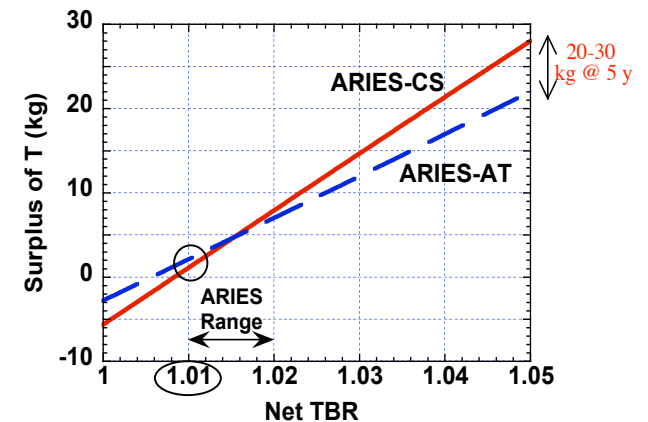
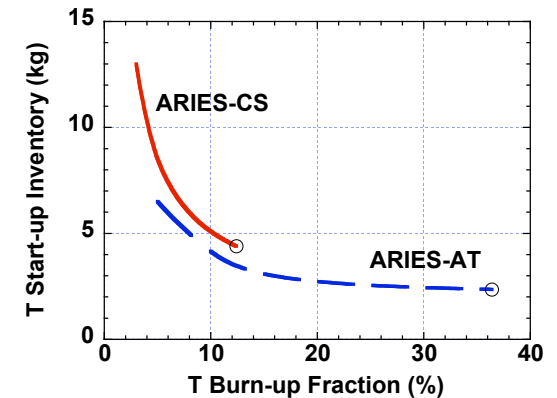
⇒ Reduce required calculated TBR from 1.1 to 1.07

LiPb obtained from Fusion for Energy had much lower lithium content (0.28 wt%) than expected for  $\text{Li}_{17}\text{Pb}_{83}$  (0.68 wt%).



# Plasma Burn-up Fraction Has **NO** Major Impact on “Excess T” Bred for Start-up of New ARIES-AT-type Plant

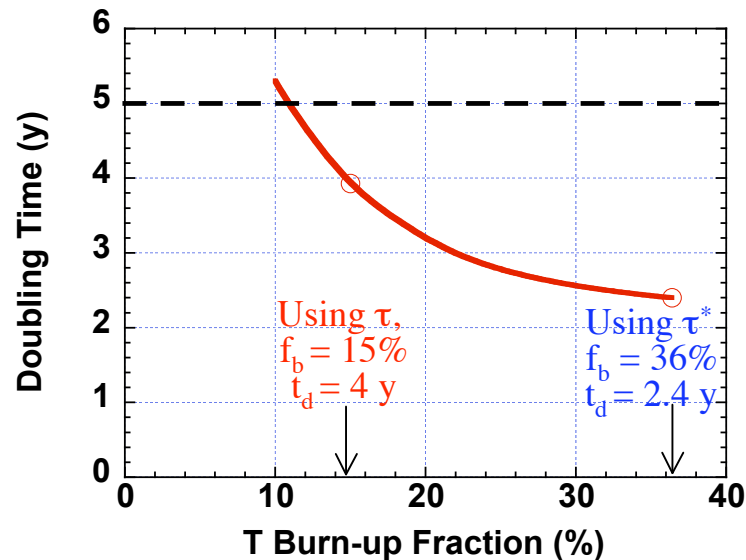
- Startup inventory of T for new power plant depends on burn-up fraction ( $f_b$ ).
- Low  $f_b$  means:
  - High startup inventory, or
  - Long doubling time ( $t_d = 1-5y$ ) (defined as time needed to supply new power plant with start-up T).
- If new design calls for lower  $f_b$ , ARIES prefers using  $t_d$  as knob to meet breeding requirements.
- Generating excessive T causes serious storage problem and raises licensing concerns.
- Note that:
  - CANDUE will produce 25 kg of T by 2025
  - Currently, PPPL is licensed for only 5 g of T
  - 4 kg of T in ITER, per N. Taylor.





## Plasma Burn-up Fraction Has **NO** Major Impact on “Excess T” Bred for Start-up of New ARIES-AT-type Plant (Cont.)

- Per C. Kessel:
  - $f_b$  is proportional to “particle confinement time” ( $\tau$ ) [difference between time of T injected into plasma and time of T lost out of plasma].
  - $\tau^*$  accounts for recycling of T from walls back into plasma.
  - $\tau^* > \tau$ .
- Which confinement time should we use to estimate  $t_d$ ?  $\tau$  or  $\tau^*$ ?
- In ARIES-AT, we used  $\tau^*$ :  $f_b = 36\%$  and  $t_d = 2.4$  y.
- Using  $\tau$ ,  $f_b = 15\%$  and  $t_d = 4$  y (still  $< 5$  y).



ARIES-AT  
Net TBR= 1.01





# Net TBR Comparison: ARIES vs UCLA

No realistic blanket design  
can breed that much T

Calculated TBR > 1.25

Nuclear Data (6-15%)

Modeling > 3%

T surplus ~ 50 kg !  
High Net TBR causes  
serious T storage and  
licensing problems

Net TBR ~ 1.15

for:  $f_b \sim 5\%$

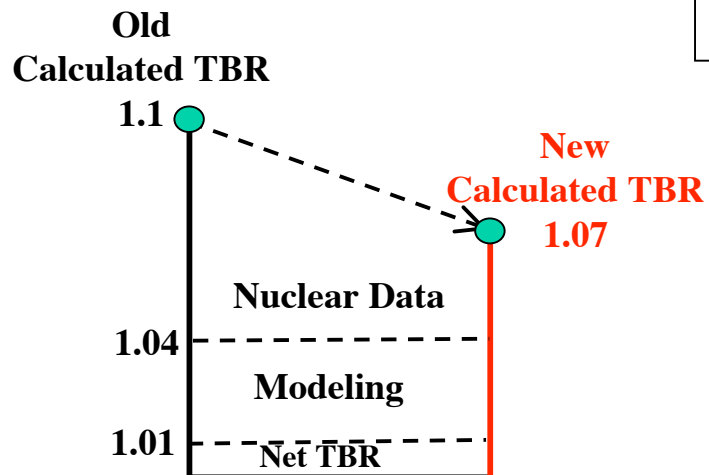
$t_d = 5$  y

2 d T reserve

1.5 GW  $P_f$

(~ 6 kg to fuel new plant)

UCLA



ARIES  
(LiPb System)



# Remarks on TBR Requirements

- Serious effort should be made to **reduce breeding requirements** (i.e., Net TBR and all uncertainties).
- Unnecessary high breeding requirements already drew criticism for fusion.
- **M. Dittmar (Zurich) reported** in “The Oil Drum: Europe (11/10/09):
  - The list of fusion problems is already very long and shows that the belief in a self-sufficient tritium chain in completely unfounded
  - Experiments show that measured TBR results are consistently ~15% lower than the modeling predicts (Sawan and Abdou FED paper, 2006)
  - One might conclude that today’s experiments show consistently that no window for self-sufficient breeding currently exists and suggest that proposal that speak of future T breeding are based on nothing more than hopes, fantasies, misunderstandings, or even international misrepresentations.
- **Advanced physics and technology should reduce breeding margin below 7%,** (as ARIES suggests) through:
  - High burn-up fraction > 10%
  - More accurate measurement of LiPb TPR
  - Careful choice of design elements that degrade breeding (FW thickness, stabilizing shell materials and location, etc.)
  - State-of-the-art 3-D neutronics models using CAD-MCNP interface.



# Li<sub>17</sub>Pb<sub>83</sub> or Li<sub>15.7</sub>Pb<sub>84.3</sub> ?

## Reference:

P. Hubberstey et al., “Is Pb-17Li really the eutectic alloy? A redetermination of the lead-rich section of the Pb-Li phase diagram ( $0.0 < x_{\text{Li}}(\text{at}\%) < 22.1$ ),”  
Journal of Nuclear Materials 191-194 (1992) 283-287.

- Single LiPb liquid phase is maintained over wide range from 13.7 to 18 at% Li.
- *LiPb eutectic lies at 15.7 at% Li, not 17 at%.*
- T solubility in LiPb is sensitive to Li content.
- Should ARIES-DCLL design consider Li<sub>15.7</sub>Pb<sub>84.3</sub> instead of Li<sub>17</sub>Pb<sub>83</sub> ?
- If so, its *minor* impact on TBR will be determined.

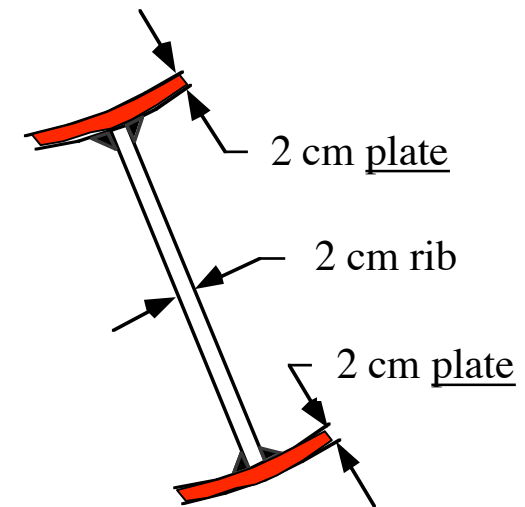
# ITER Reweldability Limits for 316-SS

< 1 He appm for **thick plate** welding

< 3 He appm for **thin plate** or **tube** welding

**Reference:** ITER Nuclear Analysis Report G 73 DDD 2 01-06-06 W 0.1 - Section 2.5.1, page 15.

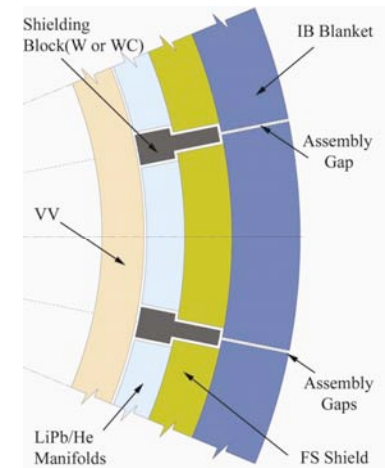
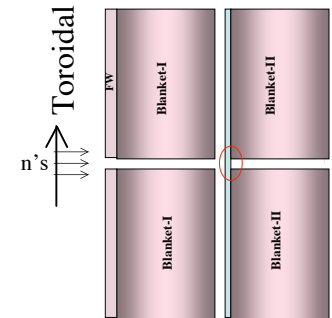
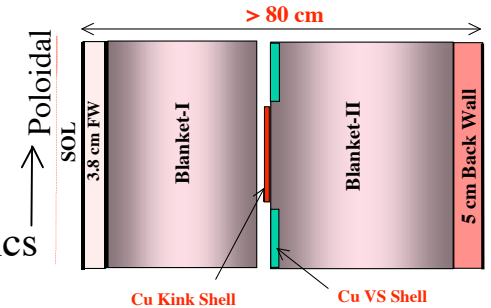
- Double-walled vacuum vessel with internal ribs:
  - ITER: **6 cm** plate of 316-SS and 1 appm limit
  - ARIES: **2 cm** plate of FS and 1 appm limit.
- Should ARIES:
  - Adopt ITER higher limit for thinner FS plate? or,
  - Revisit ARIES VV design?



ARIES-AT VV

# Segmentation of OB DCLL Blanket

- T breeding calls for fairly thick OB blanket (80 cm).
- Possible location for OB stabilizing shell is behind OB blanket (undesirable for advanced physics).
- **Advantages of blanket segmentation:**
  - Place stabilizing shells between blanket segments to enhance physics
  - Replace outer segment less frequently:
    - Reduce replacement cost
    - Minimize radwaste stream.
- **Concerns:**
  - Neutron streaming through assembly gap shortens lifetime of outer segment
  - Sensitivity of stabilizing shells to n streaming (swelling, electric resistivity, etc.)
- **Suggestion:**
  - Provide right-angle bend gaps with WC shield insert (as proposed for IB).
- **Question:**
  - How to protect toroidally continuous IB & OB shells against streaming neutrons?
- Several **iterations between physics and engineering** will determine:
  - Optimum IB & OB shell locations
  - Size of OB blanket segments
  - Impact of shells on TBR.



# Degradation of Physical Properties with Neutron Irradiation – Few Examples

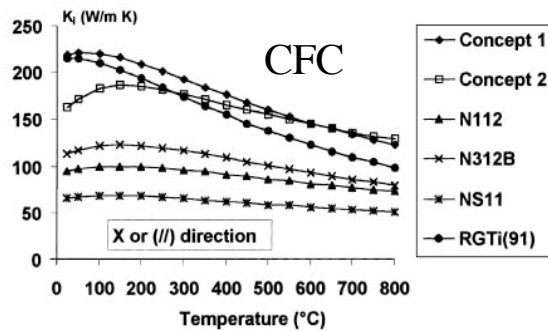


Fig. 3. Thermal conductivity of the materials as a function of the temperature after irradiation at 775°C/0.35 dpa g.

Ref.: Neutron Irradiation Effects on Carbon Based Materials at 350°C and 800°C, J.P. Bonal, C.H. Wu, *Journal of Nuclear Materials*, 277 (2000) 351-359.

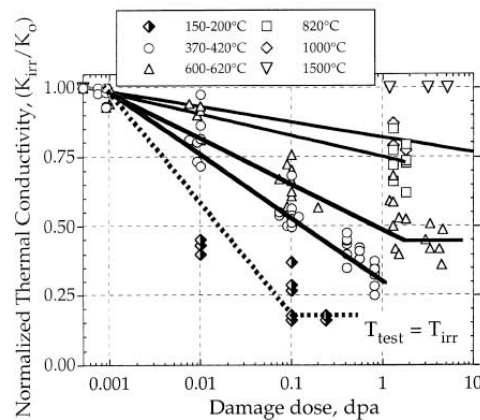


Fig. 4. Normalised thermal conductivity of different CFCs as a function of damage dose [45,53,59-63].

Ref.: Neutron Irradiation Effects on Plasma Facing Materials, V. Barabash et al., *Journal of Nuclear Materials*, 283-287 (2000) 138-146.

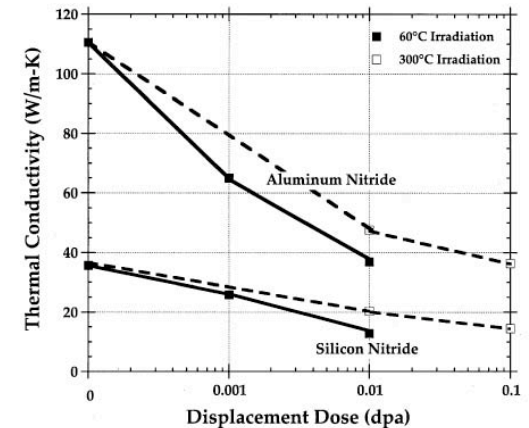


Fig. 3. Thermal conductivity vs. neutron dose for polycrystalline  $Si_3N_4$  and AlN irradiated at either 60 °C or 300 °C.

Ref.: Thermal conductivity degradation of ceramic materials due to low temperature, low dose neutron irradiation, L.L. Snead, S.J. Zinkle, D.P. White, *Journal of Nuclear Materials*, Volume 340, Issues 2-3, 15 April 2005, Pages 187-202

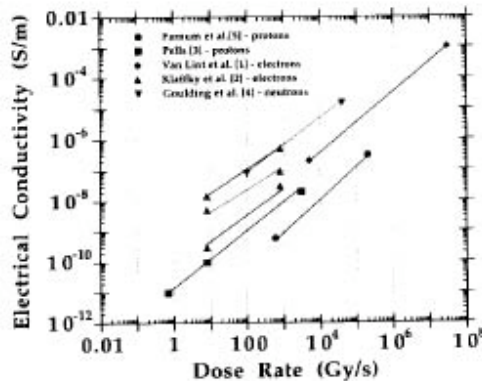


Fig. 1. Radiation induced conductivity measured in alumina during electron [1,2], proton [3,5] and fission neutron [4] irradiation.

Ref.: Investigation of Radiation Induced Electrical Degradation in Alumina Under ITER-Relevant Conditions  
L.L. Snead et al., *Journal of Nuclear Materials*, 226 (1995) 58-66

- Available data show consistent degradation of thermal and electric properties with irradiation.
- Most published data are for ITER's materials irradiated at low fluences.
- No data available for ARIES materials at high fluences of power plants.
- ARIES analysis should consider some degradation of thermal and electric properties. How much?