

# UW IEC Group 2011: Continuing Preparations for 300 kV Operation – Device Switching

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*U.S. -- Japan 2011 IEC Workshop  
Sydney, New South Wales, Australia*

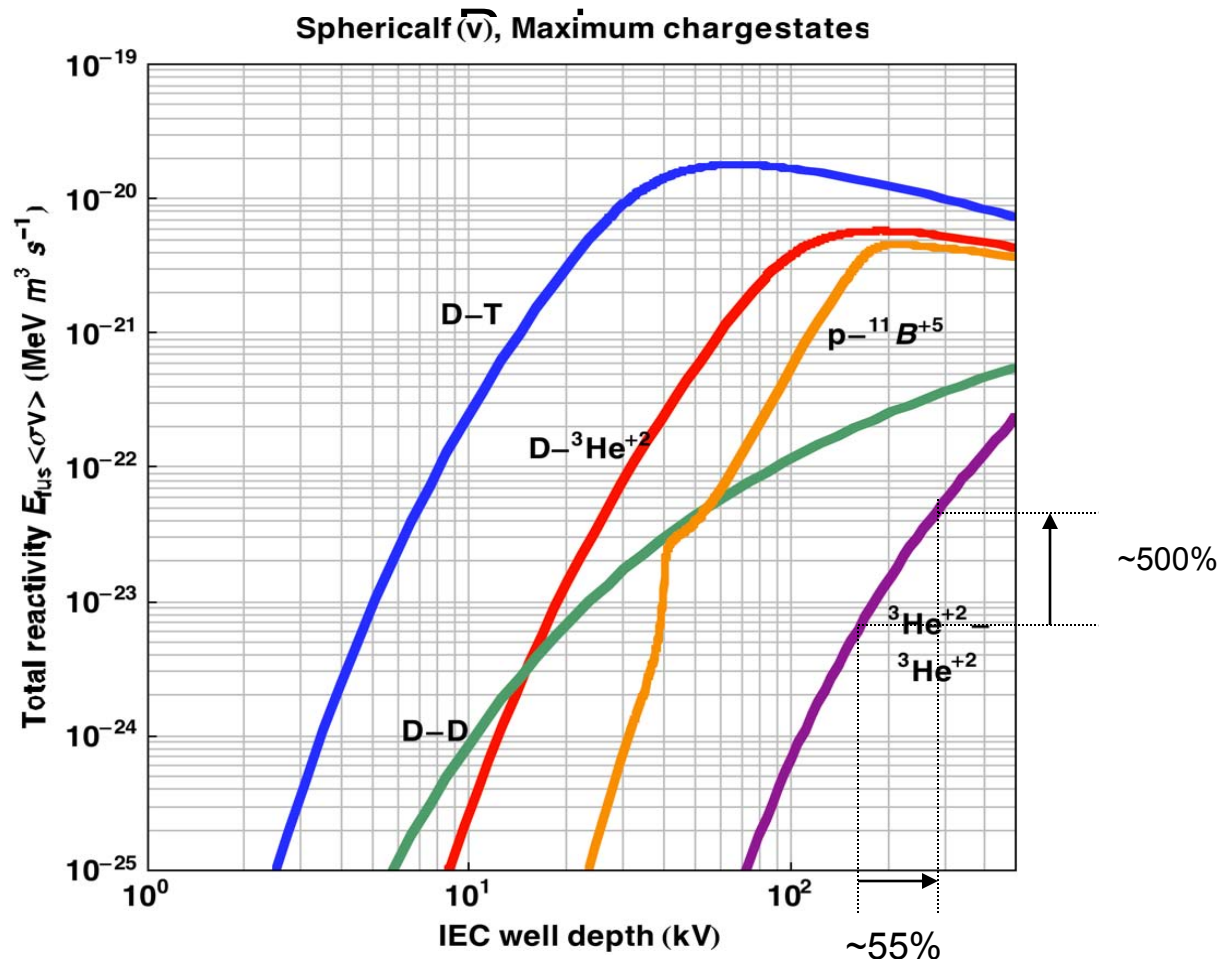
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# Motivation for Using Greater Cathode Voltages

## Improved access to ${}^3\text{He}$ - ${}^3\text{He}$ Fusion



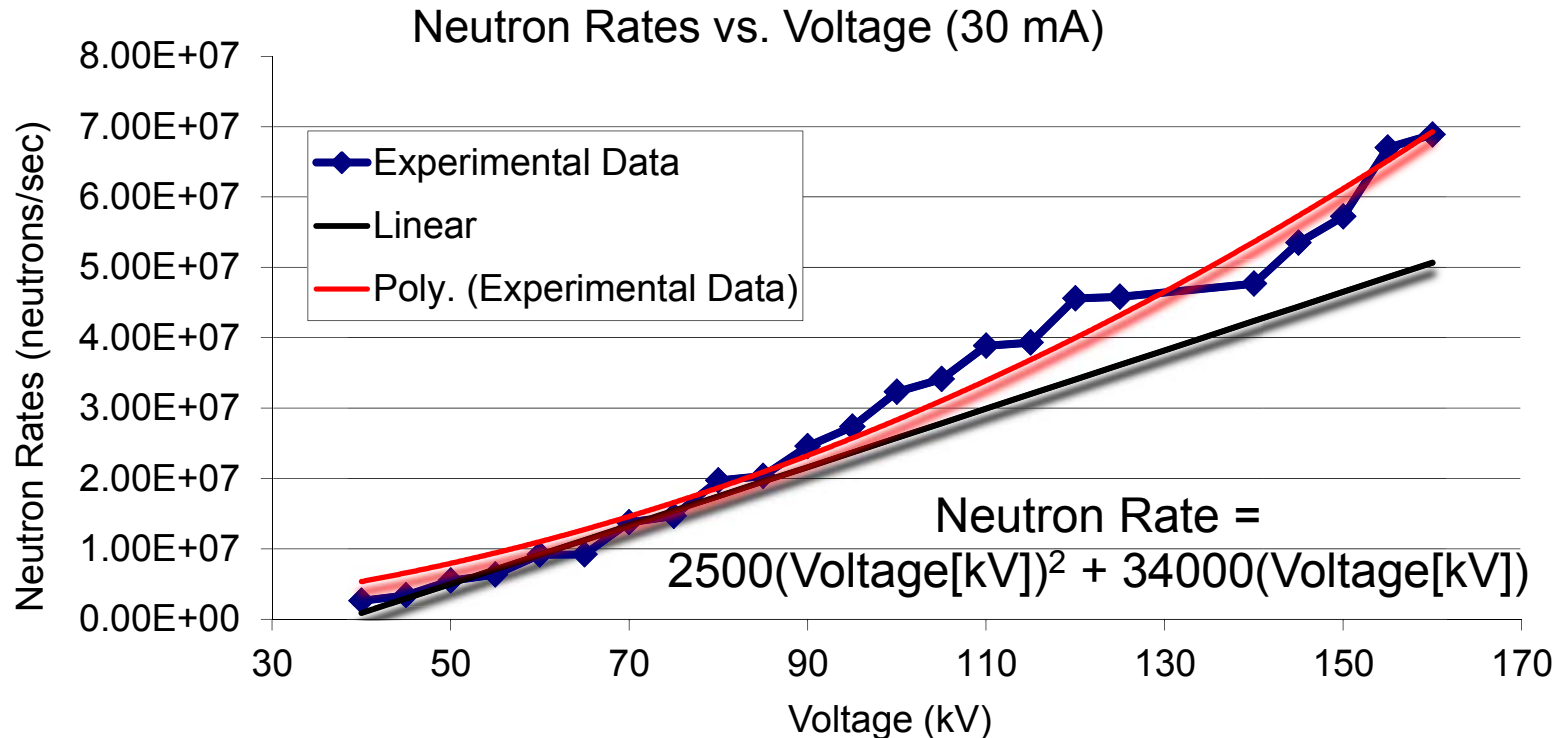
Source: J. F. Santarius



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# Motivation for Using Greater Cathode Voltages

- Neutron flux appears to be monotonically increasing with voltage (greater voltage ==> more neutrons)



From 2008 Workshop Donovan presentation (WE-08)



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# Adaptations for 300 kVDC

Completed:

- Power Supply upgrade (done)
- Vacuum Feed-through assemblies  
(covered by Becerra during this workshop)

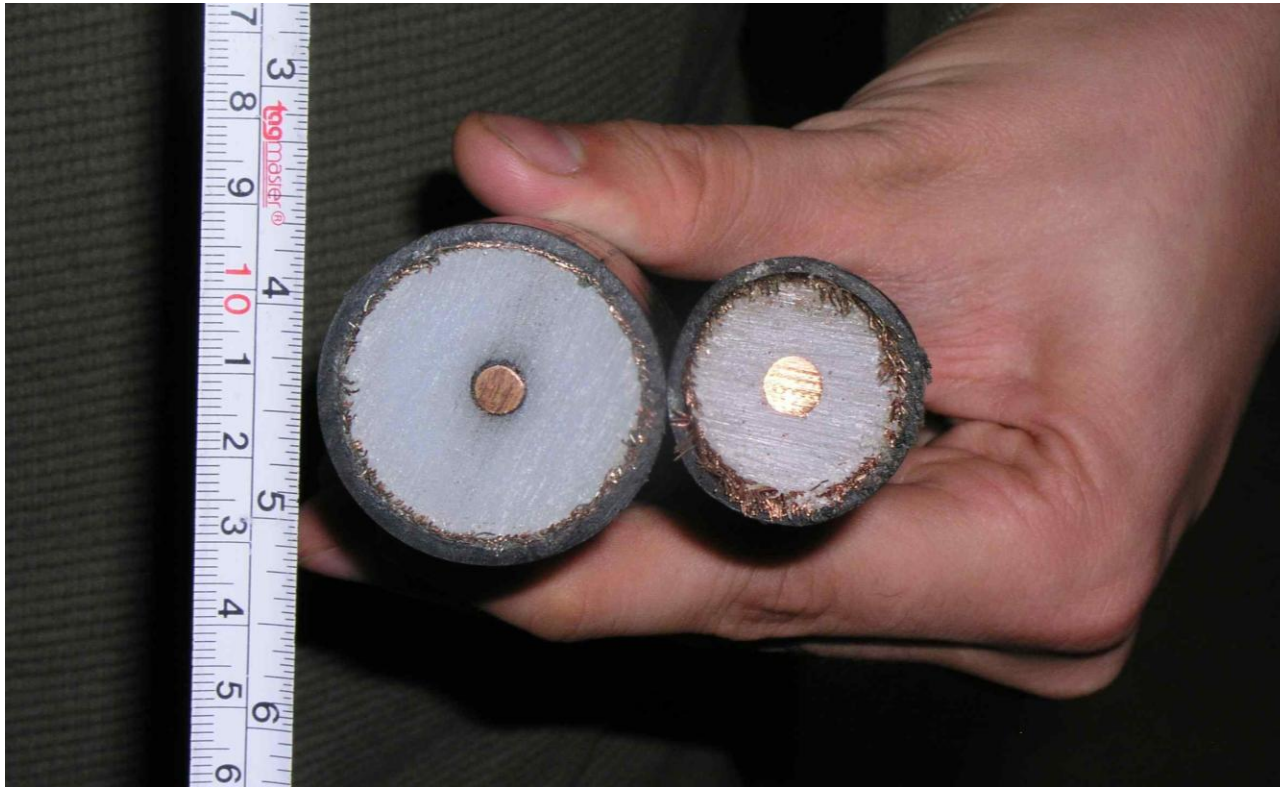
In Progress:

- Cabling
- Series Resistance assembly (“resistor barrel”)
- Switching



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# Cabling



(New) 300 kVDC cable, left, and (current) 200 kVDC cable, right

*The new cable is much less flexible, and more subject to flexure-induced failures.*



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# High Voltage Switch and Series Resistance Assembly

## Specifications:

1. Cold-switch the high-voltage power supply between four different devices
2. Removing and replacing cables not to be required
3. Non-inductive series resistor of 50 k $\Omega$  able to carry 200 mA current in steady state
4. Resistor to be adjustable to higher resistances (though at a lower current), and completely bypassable
5. Pulsing capacitor and related equipment is to be in the same enclosure as the switch.



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# Switch Design Drivers

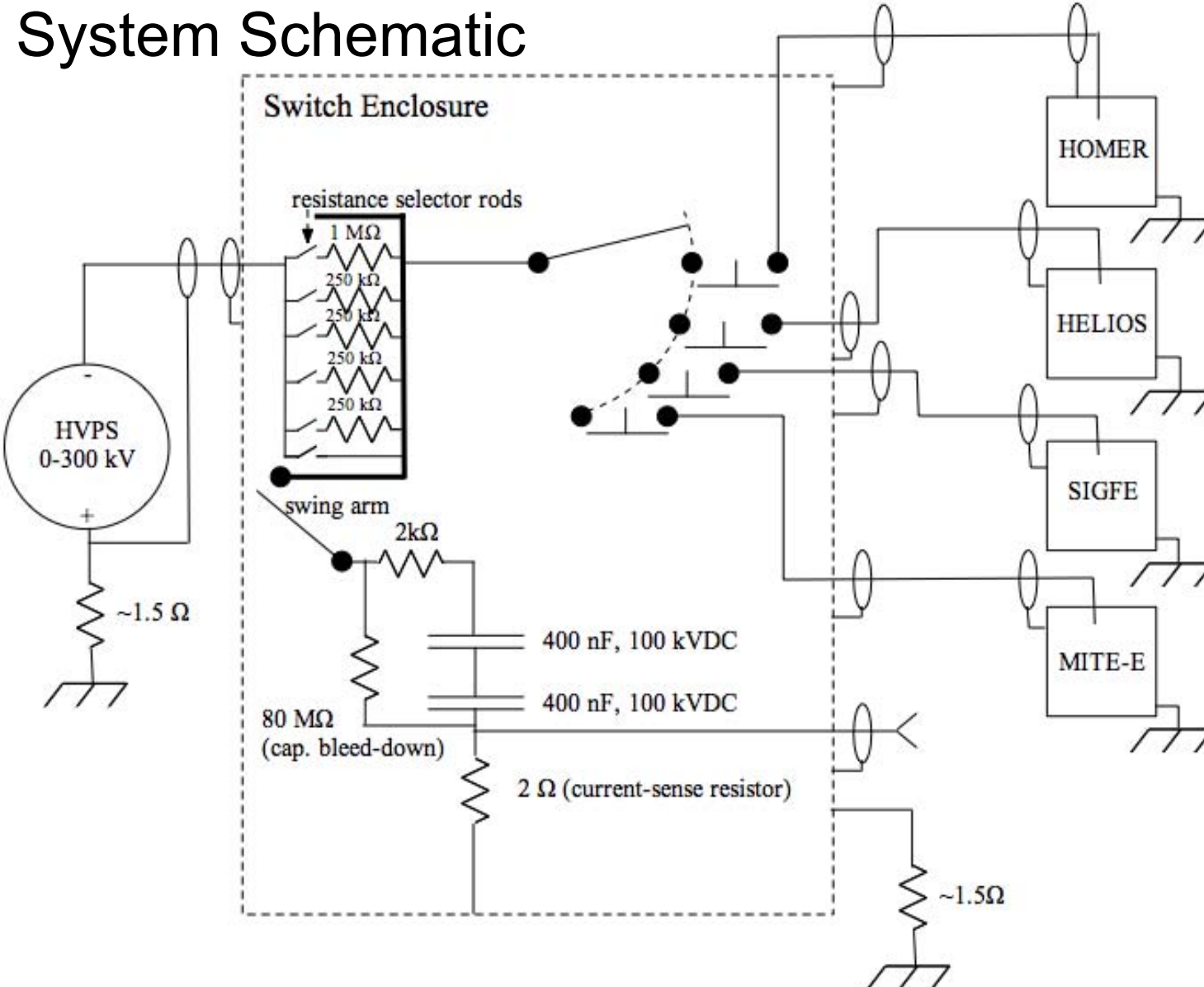
- 35 cm path length between 300 kV surface and ground (to prevent track arcing)
- 15 cm (oil filled) distance between 300 kV surface and ground (to prevent through-oil arcing)
- Electric field below  $\sim 5$  MV/m
- Resistor System requires electrostatic shielding
- Capacitor system switched in parallel with power supply for pulsing



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# System Schematic

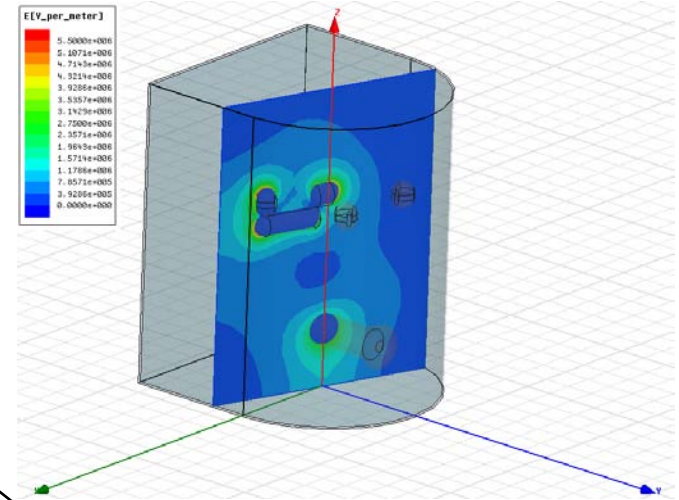
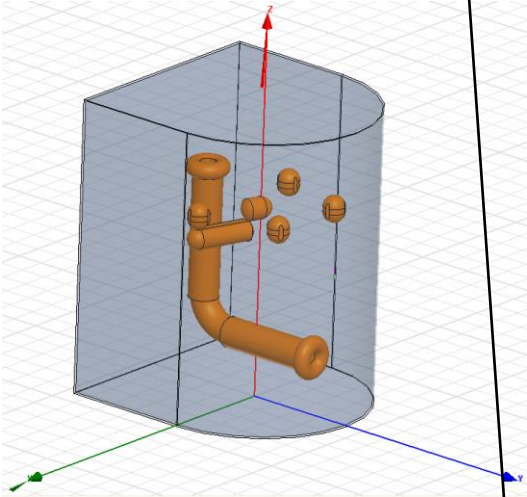


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# Design & Construction methodology

Design/Redesign  
Concept



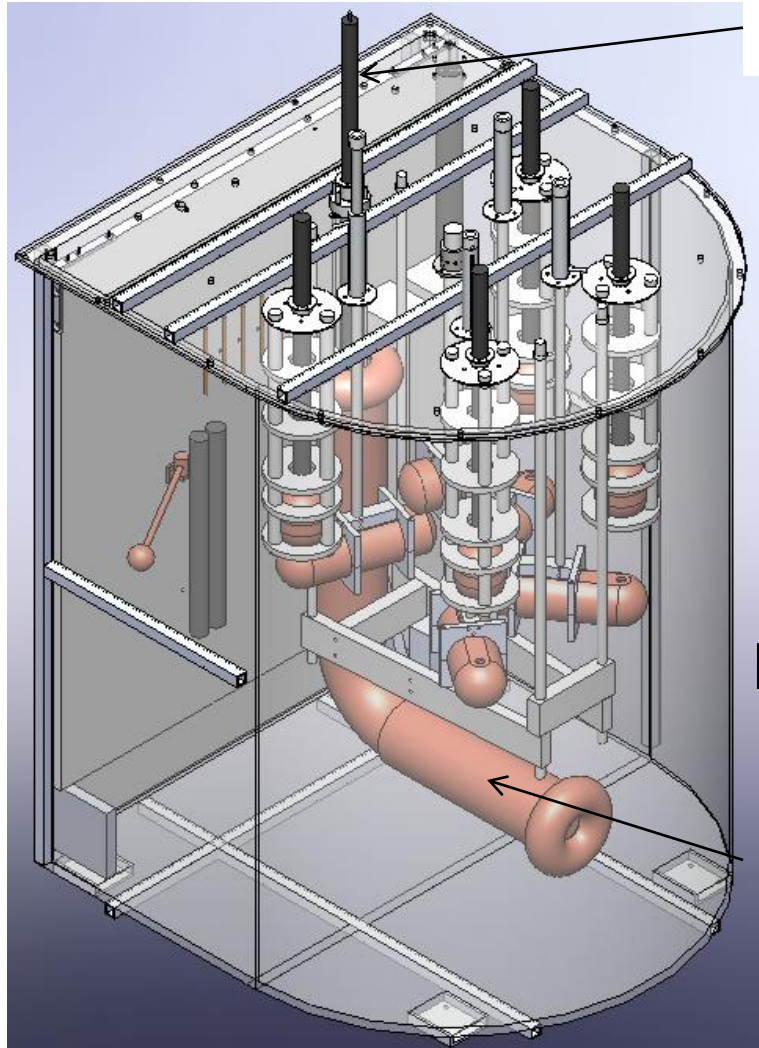
Simulation (MAXWELL  
-3D)

Construct → Test ↔ Modify

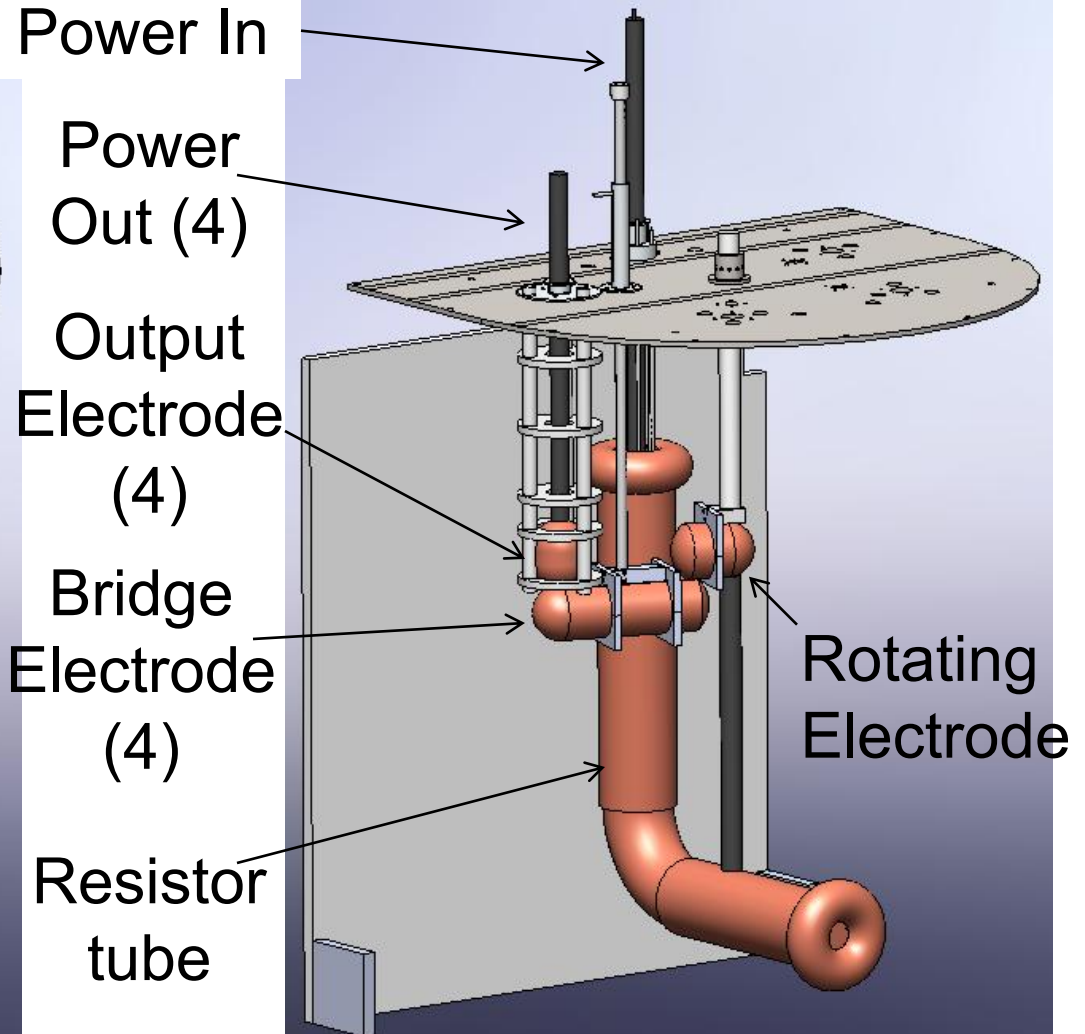


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# Final System Layout

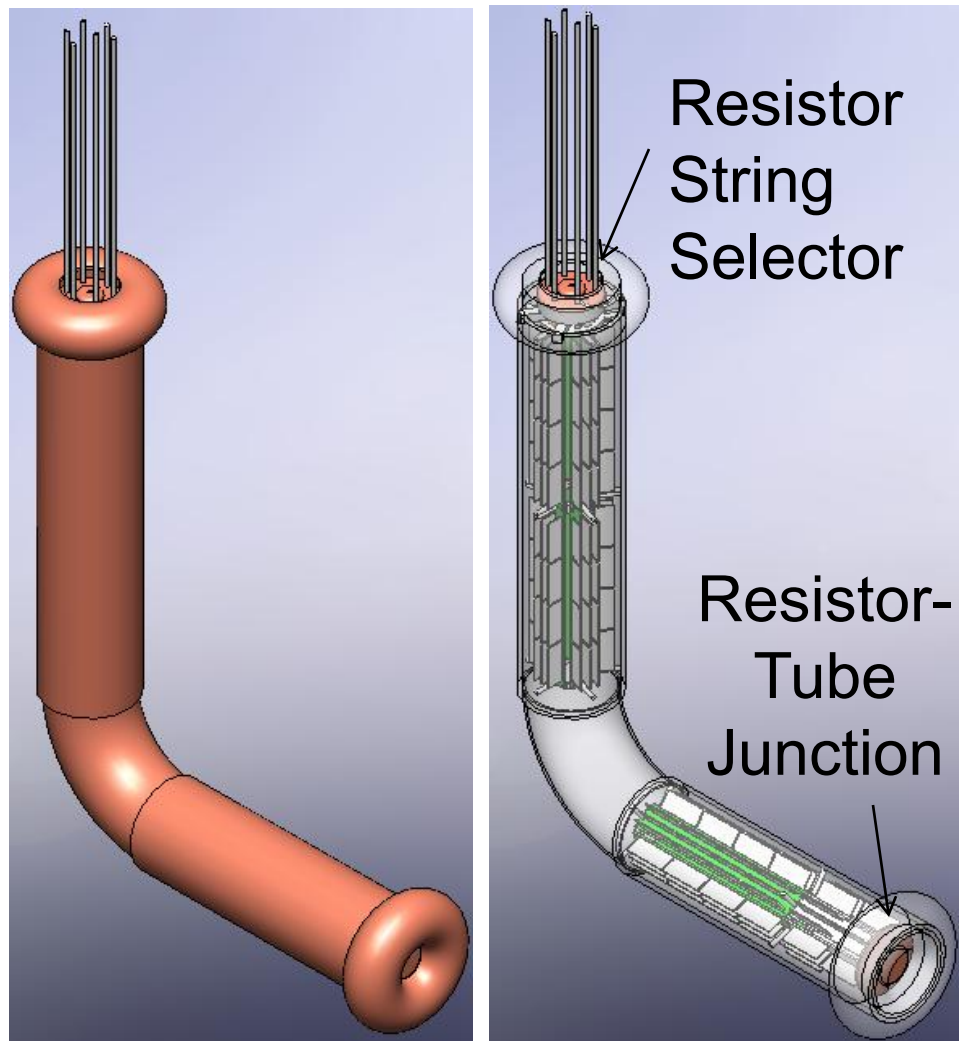


# Switching Electrodes

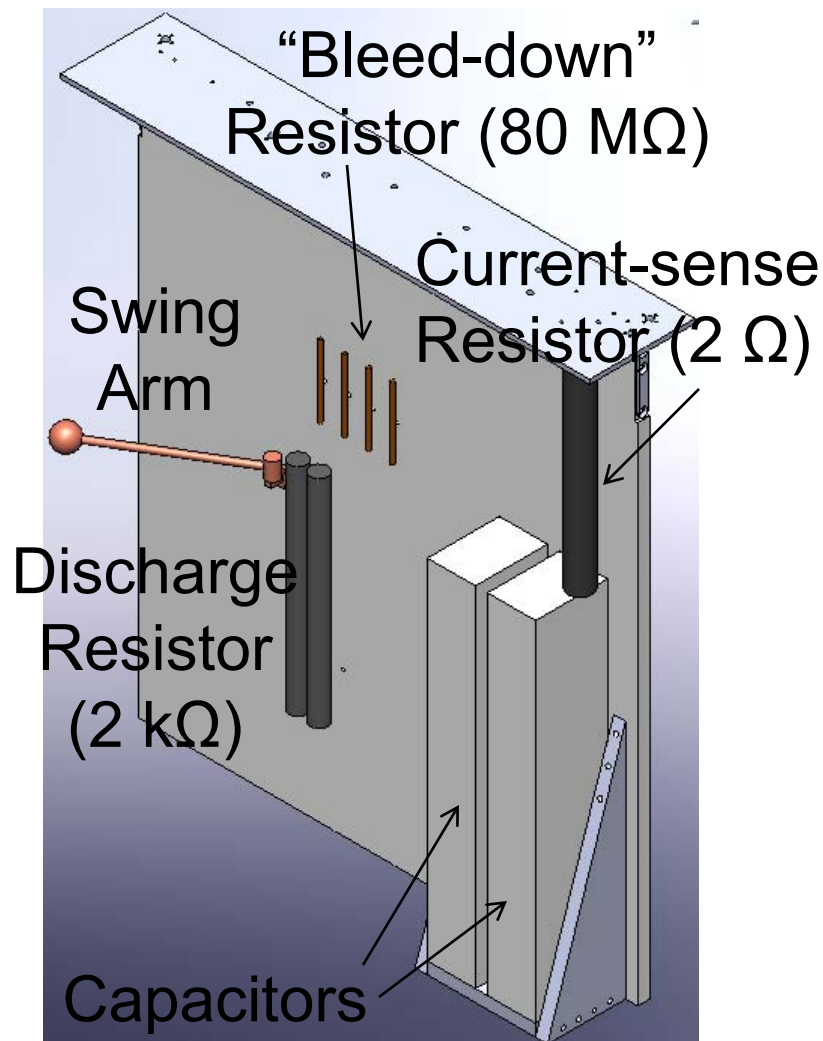


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# Resistor System



# Capacitor System



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# Manufacturing – Internal Components



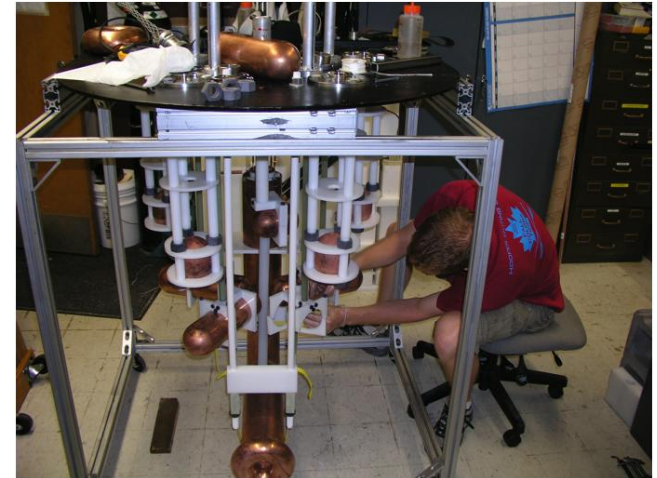
Electrodes (5 types)



Support components  
(and electrodes)



Series Resistor Strings



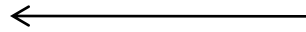
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# Manufacturing – External Components (Tank)

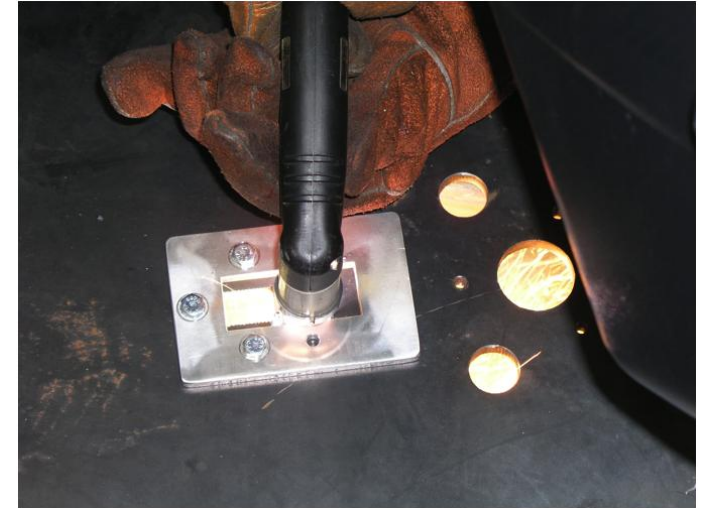
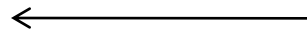
Tank Body Volume  
~ 1200 L



Removing scale



Leak Checking  
(note red dye)



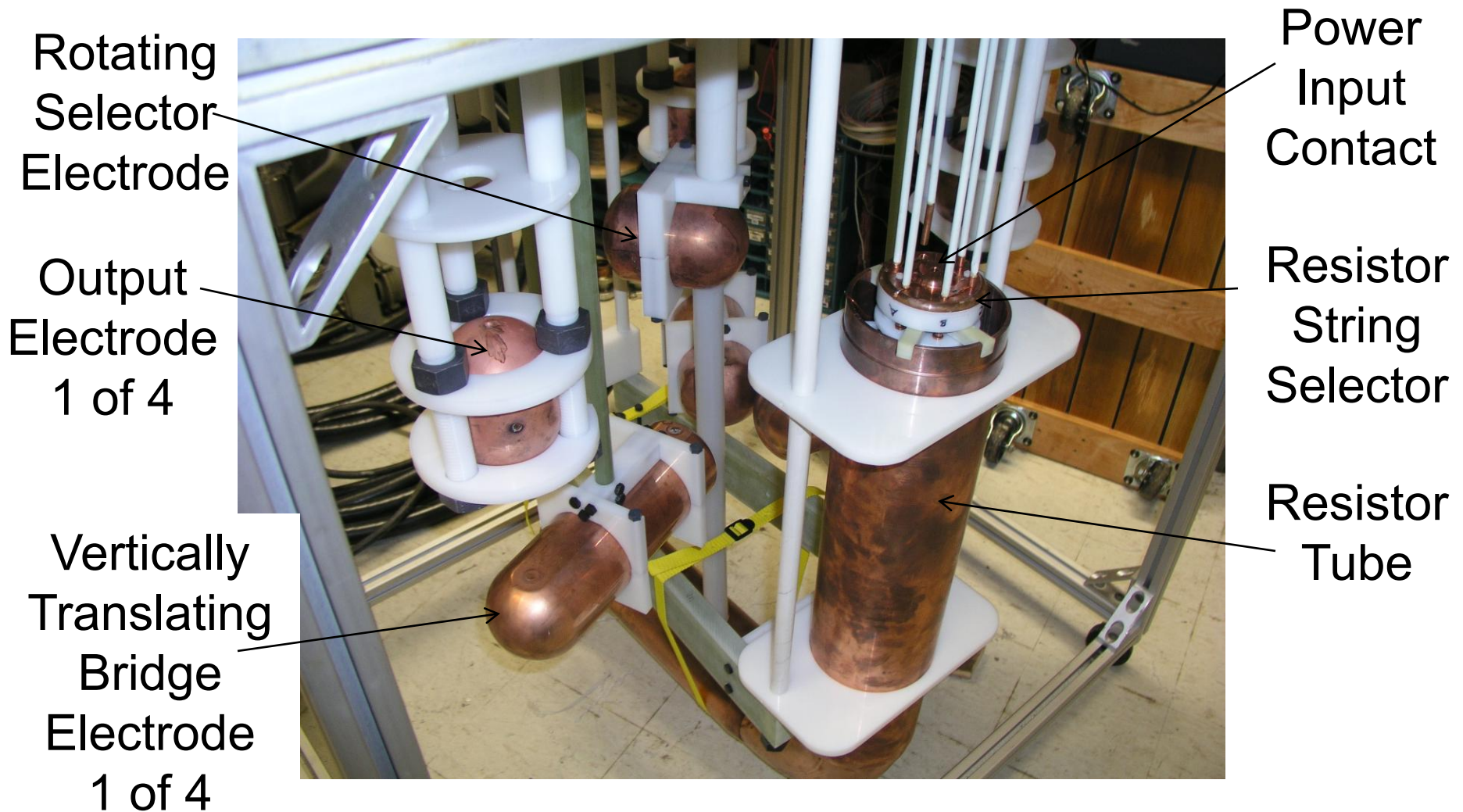
Plasma Cutting  
Slot into Lid



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# Implementation: Electrode Assembly

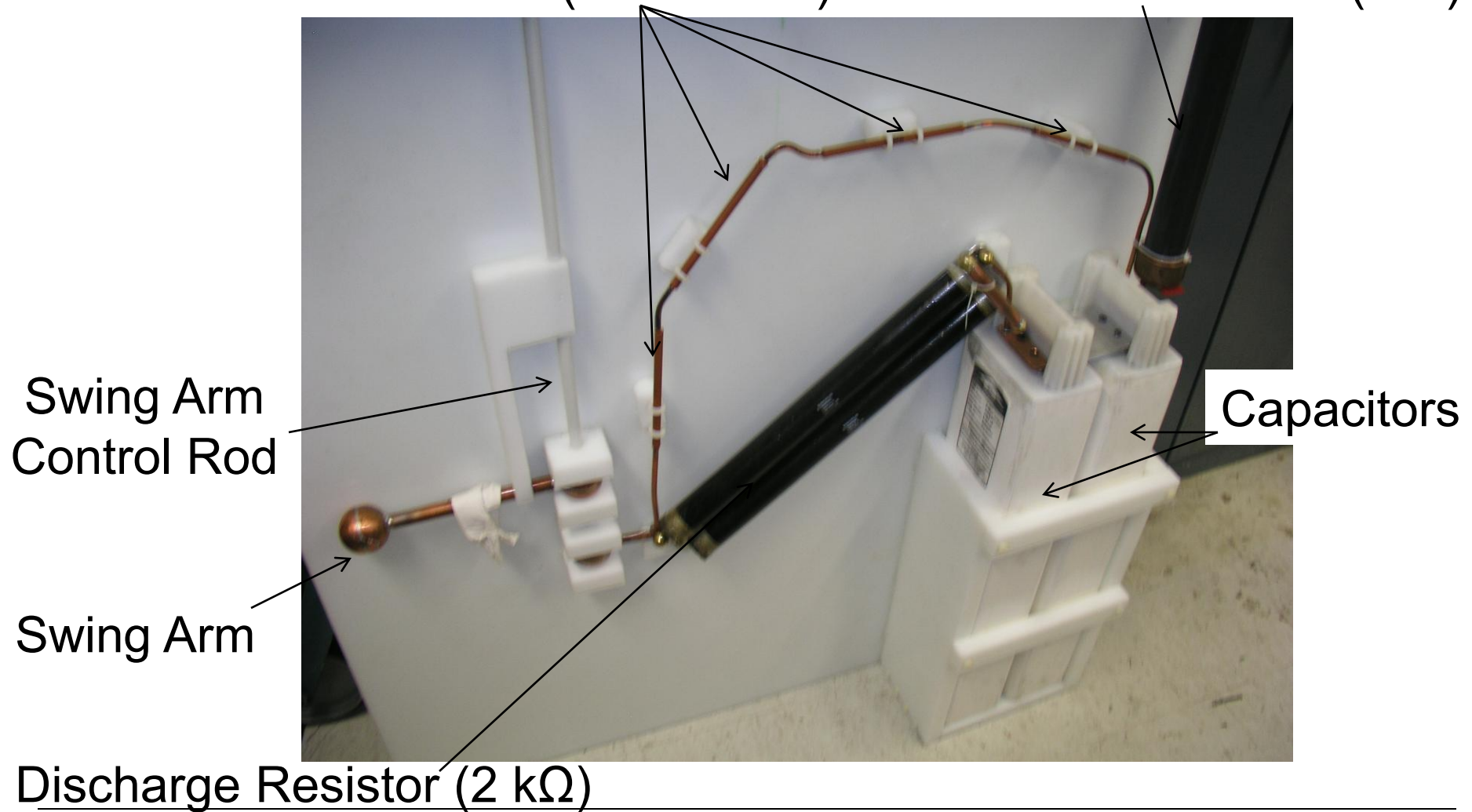


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# Implementation: Pulsing

“Bleed-Down” Resistor (4 X 20 M $\Omega$ )      Current Sense Res. (2  $\Omega$ )



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# Testing: Resistor Assembly



Initial Testing Failure: Internal Arc (corrected later)



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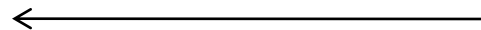


# Final Assembly

Installation of the  
pulsed system in the  
switch tank —————→

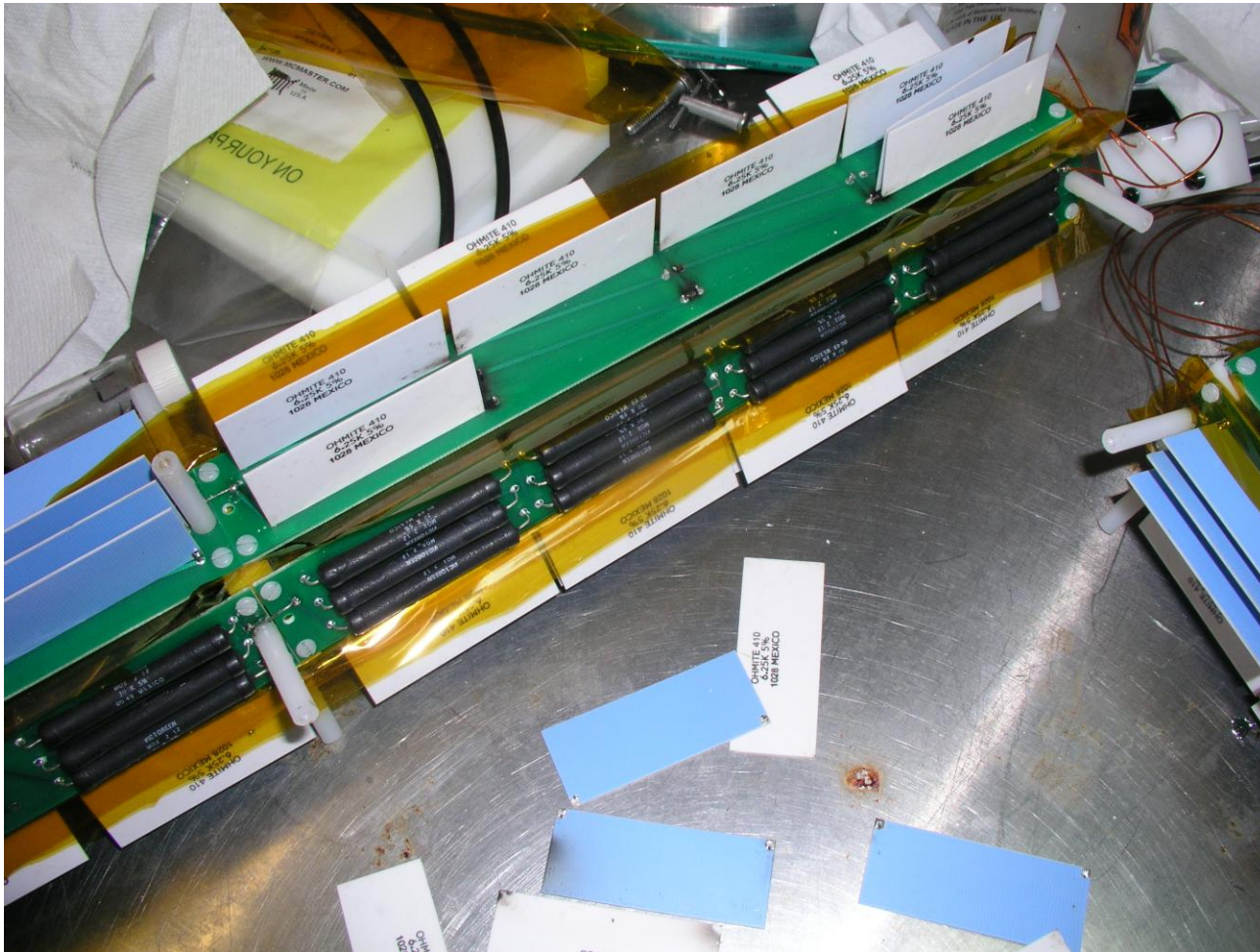


Photo of main switch  
assembly being lowered  
into switch tank



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# Testing: Resistor Assembly



Initial Testing Failure: Insufficient Cooling (later corrected)

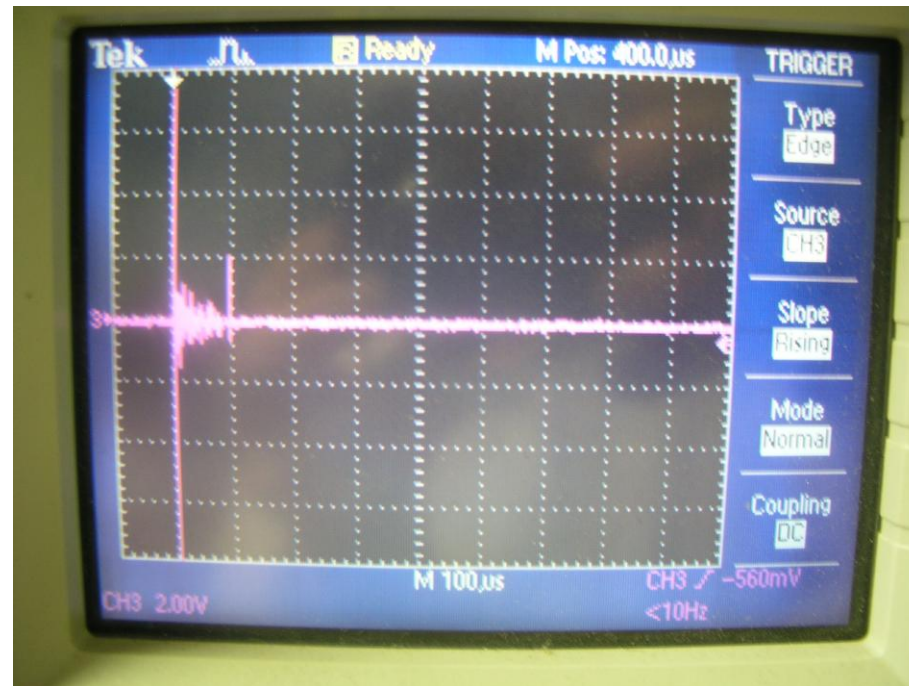


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# System Testing: High-Potential Test to 100 kV Without Dielectric Oil

Result: Unexpected, very short-time-scale arcs occurred in IEC devices when they were connected via the new switch, but not otherwise!

Vertical scale is  
1 A / division:  
arc peak current  
is off scale!



Arc duration  
is approx.  
100  $\mu$ sec.



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# Testing Results Summary:

- OK: The resistor string assemblies, as modified, can withstand the anticipated voltages and currents that are expected in regular operation.
- OK: The resistor string assemblies, when immersed in oil, will not exceed their temperature limits.
- OK: The assembled switch has been tested to 100 kV DC in air, which implies that it will likely be able to work at 300 kV DC when immersed in oil.
- **FAIL:** When an IEC device is connected through the new switch, arcing within the device occurs at 60 kV DC. **This does not occur when the device is connected via the present resistor barrel.**



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Why are these “micro-arcs” in our IEC devices not seen when we use our present (designed for 200 kV DC) resistor barrel?



Present Resistor Barrel – internal components exposed



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It is our “working assumption” that some electrical characteristic of the present resistor barrel prevents these arcs.

We are attempting to determine what this characteristic is in order that we might incorporate it into the new switch

Analytic procedure (in progress):

1. Make measurements of overall impedance characteristics, i.e.,  $|Z|$  at various frequencies
2. Attempt to fit the observed characteristics with a lumped parameter model
3. If unsuccessful, adjust the model and attempt a fit again.



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## Summary of Current Status:

- Switch components have been built and successfully tested
- System-level testing of the assembled switch failed with a peculiar “micro-arcing” which occurs in our IEC devices when powered through the new switch, but not through the present resistor barrel.
- Analysis of the current resistor barrel is in progress



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Questions?



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