



# Computation of Chemical Equilibrium in a Constant Temperature and Pressure System

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# **Computation of Chemical Equilibrium in a Constant Temperature and Pressure System**

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## i) Introduction

For multicomponent systems, at constant temperature and pressure, the calculation of chemical equilibrium of a system often requires the aid of a computer. This is especially true if the system contains several components and phases. A number of computational models have been developed of varying complexity to calculate the chemical equilibrium of multicomponent, multiphase systems<sup>1</sup>. The model chosen, in each instance, should depend upon the application. A system that contains many possible chemical species and phases requires a complex model. Unfortunately, the complex models tend to be application specific, each separate application requiring practically a total reformation of the model.

I have written a computer program that calculates the chemical equilibrium of modest size, multicomponent systems. For each application, the user is required to adjust a short subroutine and create a short input data file to employ the program. Thus the program is very general and easy to use. To achieve this, the program is limited to constant temperature and pressure systems. Also, the program is very inefficient in the calculation of the concentration of trace chemical species.

In this report I will describe, in detail, the mathematical derivation of the model, the general applicability of the model, and two specific applications of the model. In the first appli-

cation of the model, it is used to predict the equilibrium composition of a propane/air system at a specified temperature and pressure. The results are then compared to published results of the same problem, to help determine the accuracy of the method. In the second application of the model, it is used to predict the equilibrium composition of a  $\text{Li}_{17}\text{Pb}_{83}/\text{H}_2\text{O}$  system. This application is an attempt to model the recent HEDL large scale  $\text{Li}_{17}\text{Pb}_{83}/\text{H}_2\text{O}$  experiments.

## ii) Preliminaries

The model chosen is due to Van Zeggeren and Storey.<sup>2</sup> This model is also the basis for the chemical equilibrium subroutine in the core-melt program CORCON (the subroutine is named MLTREA). Unlike MLTREA, the program I have developed is intended to be easy to understand and employable to a wide range of problems. To achieve this, the program sacrifices efficiency. It has not been written to approach the solution quickly, especially if trace species are present, but to approach the solution at a relatively slow, methodical pace.

The Van Zeggeren and Storey model consists of a computational algorithm that finds the minimum Gibbs free energy of a system. This approach is taken because the minimum of a system's Gibbs free energy is equivalent to the chemical equilibrium of the system.<sup>3</sup> For a multicomponent system the Gibbs free energy is

$$G(p, T, n_i) = H(p, T, n_i) - S(p, T, n_i) T \quad (1)$$

$$\Rightarrow dG = \left( \frac{\partial G}{\partial T} \right)_{p, n_i} dT + \left( \frac{\partial G}{\partial p} \right)_{T, n_i} dp + \sum_i^N \left( \frac{\partial G}{\partial n_i} \right)_{p, T} dn_i \quad (2)$$

but, since<sup>4</sup>

$$\left( \frac{\partial G}{\partial T} \right)_{p, n_i} = -S \quad \text{and} \quad \left( \frac{\partial G}{\partial p} \right)_{T, n_i} = V \quad (3)$$

and defining

$$\left( \frac{\partial G}{\partial n_i} \right)_{p, T} = \mu_i \quad (4)$$

where,  $\mu_i$  = the chemical potential of species  $i$ ,

$$\Rightarrow dG = -S dT + V dp + \sum_i^N \mu_i dn_i \quad (5)$$

### iii) The Van Zeggeren and Storey Model

The Van Zeggeren and Storey model is based on a constant temperature and pressure system. Therefore the model starts with the differential form of the Gibbs free energy expressed as

$$dG = \sum_i^N \mu_i dn_i \quad (6)$$

This equation is recast in the form

$$\delta G = \sum_i^N \mu_i \delta n_i \quad (7)$$

This is done to mathematically separate the differential form of

the Gibbs free energy from the form of the Gibbs free energy used in the program. To compute the minimum Gibbs free energy, the program approaches the solution by calculating successive sets of  $\delta n_i$ , with each set generating a more negative Gibbs free energy than the previous set. The set of  $n_i$  which forms the solution must also satisfy M conditions of the form

$$\sum_i^N a_{ie} n_i = B_e \quad (8)$$

These conditions arise from the fact that in the chemical system being modelled, mass is neither created nor destroyed, but only changes its chemical form. From the initial composition of the system (the N initial chemical species masses), one obtains the masses of the M elements in the system. Thus the solution set of the masses of the chemical species must be such that the masses of the constituent elements are conserved.

Besides the mass balance constraints, the solution set  $n_i$  must satisfy one other obvious condition. Namely, the solution set must be such that

$$n_i \geq 0 \quad (9)$$

To insure that this condition is met, Van Zeggeren and Storey transform the equations by introducing a new variable  $\phi$ , defined by

$$n_i = \exp(\phi_i) \quad (10)$$

This transformation insures that  $n_i \geq 0$ . The system equations



(7) and the mass balance constraints (8) are transformed to

$$\delta G = \sum_i^N \mu_i n_i \delta \phi_i \quad (11)$$

$$\text{and } \sum_i^N a_{ie} n_i \delta \phi_i = \Delta B_e \quad (12)$$

$$\text{where } \Delta B_e = B_e - b_e \quad (13)$$

Here the  $B_e$  are the constrained elemental abundances, and the  $b_e$  are the elemental abundances which are obtained from the current values of the masses of the chemical species.

Mathematically, the program causes the computer to follow the line of steepest slope down the Gibbs free energy surface  $G(n_i)$ , usually in fairly small steps, until the minimum Gibbs free energy is found. At any given point in the search, the direction of the steepest slope is that which makes  $\delta G$  in equation (11) an extremum, subject to conditions (12) and an additional condition

$$\sum_i^N (\delta \phi_i)^2 = \sigma^2 \quad (14)$$

The size of the step taken during the calculation is given by  $\sigma$ .

Next the method of Lagrangian multipliers is applied to the transformed system equations (11) and the transformed conditions (12,14). The Lagrangian for the system is

$$\begin{aligned} L = & \sum_i^N \mu_i n_i \delta \phi_i - \sum_e^M \chi_e \left( \sum_i^N a_{ie} n_i \delta \phi_i - \Delta B_e \right) \\ & - \chi_\phi \left( \sum_i^N (\delta \phi_i)^2 - \sigma^2 \right) \end{aligned} \quad (15)$$

Here,  $\chi_e$  and  $\chi_\phi$  are the Lagrangian multipliers. The extremum of  $G$  is then given by the condition

$$\frac{\partial L}{\partial n_i} = 0 \quad (16)$$

$$\Rightarrow \mu_i n_i - \chi_\phi \delta\phi_i - \sum_e^M \chi_e a_{ie} n_i = 0 \quad (17)$$

$$\Rightarrow \delta\phi_i = \frac{n_i}{\chi_\phi} \left( \mu_i - \sum_e^M \chi_e a_{ie} \right) \quad (18)$$

Equations (18) can be used to find  $\delta\phi_i$  in terms of both known quantities and the Lagrangian multipliers. It is thus necessary to express  $\chi_e$  and  $\chi_\phi$  in terms of known quantities. This is accomplished by multiplying equations (18) by  $a_{ie}n_i$  and summing over  $i$ . Using the mass balance equations (12) this leads to  $M$  equations

$$\sum_f^M \left( \sum_i^N a_{ie} a_{if} n_i^2 \right) \chi_f = \sum_i^N a_{ie} \mu_i n_i^2 - \chi_\phi \Delta B_e \quad (19)$$

The Lagrangian multiplier  $\chi_e$  can be written as

$$\chi_e = \eta_e + \chi_\phi \omega_e \quad (20)$$

The coefficients  $\eta_e$  and  $\omega_e$  are given by the equations

$$\sum_f^M \left( \sum_i^N a_{ie} a_{if} n_i^2 \right) \eta_f = \sum_i^N a_{ie} \mu_i n_i^2 \quad (21)$$

$$\sum_f^M \left( \sum_i^N a_{ie} a_{if} n_i^2 \right) \omega_f = -\Delta B_e \quad (22)$$

Equation (18) can now be rewritten as

$$\delta\phi_i = \frac{1}{\chi_\phi} ( D_i - \chi_\phi E_i ) \quad (23)$$

$$\text{where } D_i = \mu_i n_i - \sum_e^M \omega_e a_{ie} n_i \quad (24)$$

$$E_i = \sum_e^M \omega_e a_{ie} n_i \quad (25)$$

Finally, by substituting for  $\delta\phi_i$  from equation (23) into the subsidiary condition (14) and solving for  $\chi_\phi$  leads to

$$\chi_\phi = - \left[ \left( \sum_i^N D_i^2 \right) / \left( \sigma^2 - \sum_i^N E_i^2 \right) \right]^{\frac{1}{2}} \quad (26)$$

The negative sign in this equation must be present for the procedure to minimize the Gibbs free energy.

#### iv) Computer Algorithm

The basic cycle for calculating improved estimates of the equilibrium composition consists of these steps:<sup>5</sup>

1). First the program parameters are initialized by a call to the input subroutine CHEMIN.

2). Next the species chemical potentials and the system Gibbs free energy are calculated. The species chemical potentials are given by

$$\mu_i = \mu_i^{\circ}(T) + R T \ln \left[ \epsilon_i n_i / \left( \sum_j^N \alpha_j n_j \right) \right] \quad (27)$$

where  $\epsilon_i = \frac{P}{P_0}$ , if  $n_i$  is a gas,

or  $\epsilon_i = 1$ , if  $n_i$  is a solid or liquid, (28)

and  $\alpha_j = 1$ , if species  $i$  and  $j$  are of the same phase,

or  $\alpha_j = 0$ , if species  $i$  and  $j$  are of different phases. (29)

For the applications I am considering, I use two definitions of the chemical potential at 1 atm. In the first application, the propane/air system, I use the standard definition:

$$\mu_i^{\circ} = ( \Delta G_f^{\circ}(T) )_i \quad (30)$$

Since, for the  $\text{Li}_{17}\text{Pb}_{83}$  compound, the Gibbs free energy of formation is not tabulated, I must use an alternate definition for the chemical potential of  $\text{Li}_{17}\text{Pb}_{83}$  at 1 atm. Thus for the second application, the  $\text{Li}_{17}\text{Pb}_{83}/\text{H}_2\text{O}$  system, I use the definition:

$$\mu_i^{\circ} = ( G^{\circ}(T) - H^{\circ}(298) )_i + ( \Delta H_f^{\circ}(298) )_i \quad (31)$$

Both of these expressions are equally valid, because the actual values of  $\mu_i^{\circ}$  are unimportant; only their differences are thermodynamically defined, and the selection of  $\mu_i^{\circ}$  values is based on convention only.<sup>6</sup> Values of  $\mu_i^{\circ}$  are obtained from data from the JANAF tables.<sup>7</sup>

3). Calculate the current values of  $\Delta B_e$ , using equations (12) and (13).

4). Form the sums over  $i$  appearing in equations (21) and (22).

5). Solve equations (21) and (22) to determine the coefficients  $W_e$  and  $Q_e$ . These equations are solved using the matrix inversion subroutine MATINV.

6). Find  $D_i$  and  $E_i$  from equations (24) and (25).

7). Find  $X_\phi$  from equation (26).

8). Find the set of  $\delta\phi_i$  values from equation (23).

9). Calculate new estimates of the equilibrium composition from

$$n_i = m_i \exp(\delta\phi_i) \quad (32)$$

10). Next, two convergence criteria are checked to determine whether or not the set  $n_i$  corresponds to the equilibrium composition. The first condition is; has the step size decreased to the input cutoff value? Namely, is

$$\sigma \leq \tau \quad (33)$$

The second condition is, have the the current values of the element masses converged to the constrained element masses? Namely, is

$$|B_e - b_e| \leq \epsilon B_e \quad (34)$$

11). If either of the conditions (33) or (34) are false, then the step size is adjusted, depending upon the values of  $\delta\phi_i$  from the current step and the previous step. The values of the program variables are then set to the new variable values, and

the program returns to step 2).

12). If the conditions (33) and (34) are true, then the equilibrium composition of the system has been found. The program calls the output subroutine CHOUT, and then terminates.

#### v) Program Use

To employ the program, the user needs to create a short data file and subroutine that contain the problem specific data.

The subroutine that the user needs to create is called by the name CHEMP0. It must contain formulas for the chemical potentials, at 1 atm, of each species. Also, the subroutine must specify the phase of each species. The subroutine must be written in FORTRAN. Once compiled, the subroutine can then be linked with the object file that contains the compiled form of the rest of the program (CHEMEQ.OBJ). The interested reader should refer to the program listing appendix included at the end of this report to ascertain the required format of the CHEMP0 subroutine. (This appendix contains the program listing of the two versions of CHEMP0 that I have used in the applications discussed in this paper.)

The data file that the user must create contains problem specific data, in free format form, in the following configuration. The first line of the file must contain the number of species being considered (N), and then the number of constituent

elements (M). The next N lines must contain the names of the species. Each record can contain up to 10 characters. The next M lines must contain the names of the elements. Again, each record can contain up to 10 characters. These N+M lines are not free format; the characters must be placed in the first 10 columns of each line. The order of the species and element names given in these lines will be the order maintained by the program. Namely, suppose the first record in this list is H<sub>2</sub>O, then n<sub>1</sub>, δ<sub>1</sub>, and so forth, will refer to the species H<sub>2</sub>O. Lastly, the final M lines must contain the array of stoichiometric coefficients (a<sub>ie</sub>). Each of these lines must contain N numbers. As an example: Suppose that the first element in the element portion of the data file is H. Then suppose that there are 10 species being considered. If, say, only species 1, 3, and 9 contained hydrogen, and that these species were, n<sub>1</sub> = H<sub>2</sub>O, n<sub>3</sub> = HCl, and n<sub>9</sub> = H<sub>2</sub>; then the first line of the stoichiometric array portion of the data file will be

2., 0., 1., 0., 0., 0., 0., 0., 2., 0.

The program will request that the user provide the rest of the needed input data. The program will first prompt the user to enter a program run title. It will then request that the user provide it with the system temperature and pressure for that run. The user will then be asked to give the initial mass (in mole) of the problem species. The program then reports the default values of the program conversion parameters, and asks whether or not the user wants to change these parameters. The parameters that the

user has the power to adjust are: the initial step size, the minimum step size convergence parameter, the mass balance constraint convergence parameter, and the trace species cutoff parameter.

#### vi) The Propane/Air System Application

The model is first applied to a propane/air system. Specifically, the model is used to predict the results of the combustion of propane with air, to give decomposition products, at 2200 K and 40 atm. The only system parameter considered is the molar ratio  $R$  of air ( $O_2 + 4N_2$ ) to propane ( $C_3H_8$ ). The chemical equilibrium of this system is chosen because the Van Zeggeren and Storey used this problem to calibrate their models. The results of this analysis are tabulated on the next page. The data in this table are in mole fractions:  $x_i = n_i / n$ , where  $n = \sum n_g$  (i.e., the sum of the molar masses of the gases in the equilibrium system). The first number in presented is taken from the literature.<sup>9</sup>



## Comparison of the Results from the Model with the Literature

For the Reaction:  $\text{C}_3\text{H}_8 + \text{R} (\text{O}_2 + 4\text{N}_2) \Rightarrow \text{Products}$ 

Products	R = 1		R = 2		R = 5	
	Lit.	Model	Lit.	Model	Lit.	Model
$\text{CO}_2$	0.00002	1.75E-5	0.00989	0.00988	0.10795	0.10797
$\text{N}_2$	0.39996	0.39996	0.53322	0.53322	0.73874	0.73874
$\text{H}_2\text{O}$	0.00018	1.82E-4	0.05675	0.05675	0.14674	0.14674
$\text{CO}$	0.19976	0.19976	0.19006	0.19007	0.00294	2.93E-3
$\text{H}_2$	0.39953	0.39953	0.20966	0.20966	0.00077	7.65E-4
$\text{H}$	0.00056	5.61E-4	0.00041	4.06E-4	0.00002	2.45E-5
$\text{OH}$	0.00000	6.20E-8	0.00002	1.53E-5	0.00068	6.74E-4
$\text{O}$	0.00000	0.00000	0.00000	3.83E-7	0.00001	1.27E-5
$\text{NO}$	0.00000	2.15E-8	0.00000	1.64E-6	0.00097	9.75E-4
$\text{O}_2$	0.00000	0.00000	0.00000	0.00000	0.00119	0.00119
$\text{C}$	0.10020	0.10020	0.00000	0.00000	0.00000	0.00000

As the table shows, the program predicts the same equilibrium composition as is given in the Van Zeggeren and Storey text. Thus one can conclude that the program is as effective as the program written by Van Zeggeren and Storey. As can be seen, the program produces data that is as accurate as the published data. But this is only because I experimented with the program parameters until the program would produce the desired accurate results. This means that the user has control over the accuracy of the program output. The parameter that provides the user with this ability is the trace species cutoff parameter.

The program is endowed with the ability to set the mass of certain trace species to zero, and thus increase the speed at which the program converges to the equilibrium composition. The program accomplishes this feat in the following manner. Early in the execution of the program, the maximum possible species mass, which is determined from the contained element masses, is calculated. If the ratio of the current species mass to the maximum species mass ever falls below the species cutoff parameter, then that species mass is set equal to zero. Thus if the user sets the species cutoff parameter to a relatively high value, the program will execute quickly. But, the user will then run the risk of having the program predict a final composition that is not near the true equilibrium composition. On the other hand, if the user sets the trace species cutoff parameter to a relatively small value, the program execution time may increase to a prohibitively high amount.

The best way to determine an adequate setting for the trace species cutoff parameter is to experiment. At first application of the program, the user should set the trace species cutoff parameter to a very low value. Since the program writes the species composition to the screen after every 10 iterations, one can monitor the action of the program. Typically, some species will converge quickly to relatively high masses. Other species will quickly reach relatively small mass values, but will not converge to any value. They will instead, continue to decrease in value, but they may take a prohibitive amount of time to converge to some value. When this happens, the user can halt execution of the program and reexecute the program with a larger value of the species cutoff parameter. Using this method, the user will eventually find a solution that is adequate to his needs. As an example, the data for the  $R = 1$  column in the above table took 2520 program iterations, with the trace species cutoff parameter set equal to  $5 * 10^{-7}$ , to determine. This took approximately 10 minutes of execution time on an IBM XT.

#### vii) The $\text{Li}_{17}\text{Pb}_{83}/\text{H}_2\text{O}$ System Application

Knowing that the program performs properly, one can now use it to determine the degree of equilibrium interaction exhibited in the data from an experiment. The data analyzed in this manner is taken from a series of large scale  $\text{Li}_{17}\text{Pb}_{83}/\text{H}_2\text{O}$  experiments<sup>10,11</sup>, carried out at the Hanford Engineering Development

Laboratory. The experiment consisted of the injection of high pressure steam into a liquid  $\text{Li}_{17}\text{Pb}_{83}$  pool. The average temperature was approximately 1140K at atmospheric pressure. Through the course of the experiment, 90.18 mole of  $\text{H}_2\text{O}$  were injected into 1155 mole of alloy. With this data, one can run the program. The predicted equilibrium composition of the system is presented on the next page.

Li-17 Pb-83 / H2O Reaction: HEDL Large-scale test parameters  
 For T = 1143. K and P = 1.0135E+05 Pa  
 The minimum Gibbs free energy = -5.6449E+07 J  
 The number of iterations = 2403

Element	Element mass [MOLE]
Li	196.350
Pb	958.650
H	180.360
O	90.1800

Species	Initial mass [MOLE]	Equilibrium mass [MOLE]
Li	68.4990	3.528763E-02
Pb	862.785	622.127
Li17Pb83	115.500	405.450
H2	54.1080	63.6941
H2O	9.01800	1.675298E-03
Li2O	27.0540	37.2100
LIOH	54.1080	52.9684

\*\*\*\*\*

Li-17 Pb-83 / H2O Reaction: HEDL Large-scale test parameters

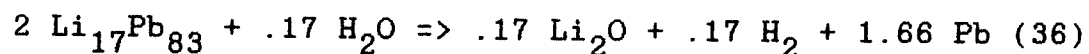
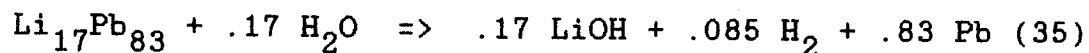
For T = 1143. K and P = 1.0135E+05 Pa  
 The minimum Gibbs free energy = -5.6449E+07 J  
 The number of iterations = 2413

Element	Element mass [MOLE]
Li	196.348
Pb	958.633
H	180.358
O	90.1790

Species	Initial mass [MOLE]	Equilibrium mass [MOLE]
Li	26.5300	3.530048E-02
Pb	910.700	622.116
Li17Pb83	57.7500	405.441
H2	80.0000	63.6936
H2O	4.50900	1.680857E-03
Li2O	74.3300	37.2098
LIOH	11.3400	52.9675

Before discussing the results of the analysis, the process of choosing an initial composition needs to be clarified. As shown on the last page, the program was executed twice, with only the initial composition varying between the two runs. If one compares the equilibrium composition of the two runs, one can see that the initial composition does not affect the program results. Although one may be led to believe that the program will perform properly regardless of the chosen initial composition, this is not the case. The user must supply the program with nonzero initial species masses. This may be a very complicated task if the number of species is much larger than the number of elements. In very simple terms, the process of choosing an initial composition can be explained in the following manner. The first step is to determine the constrained element masses. For the  $\text{Li}_{17}\text{Pb}_{83}/\text{H}_2\text{O}$  system discussed above, since we know that the experiment consisted of the mixing of 90.18 mole of  $\text{H}_2\text{O}$  and 1155 mole of  $\text{Li}_{17}\text{Pb}_{83}$ , determining the constrained element masses is relatively easy. Next the user randomly sets a few of the initial species masses to nonzero values. He can then determine the remaining species masses by a process of elimination and random setting of values. In practice, the user may find the process of choosing a suitable initial composition a difficult task, but it can be accomplished with a little patience and experimentation.

Now turning to the results of the analysis,  $\text{Li}_{17}\text{Pb}_{83}$  and  $\text{H}_2\text{O}$  react by two possible reaction paths:



Since the predicted equilibrium composition contains 52.97 mole of LiOH and 37.21 mole of Li<sub>2</sub>O, and since practically all of the 90.18 mole of H<sub>2</sub>O reacted, one can show that 41.26% of the H<sub>2</sub>O reacted by the first route (equation (35)), and 58.74% of the H<sub>2</sub>O reacted by the second route (equation(36)). But since a total of 99 mole of H<sub>2</sub> was collected during the experiment, all of the H<sub>2</sub>O reacted to form one mole of H<sub>2</sub> per mole of H<sub>2</sub>O reacted. Thus experimentally, the H<sub>2</sub>O reacted almost exclusively by the second route (equation(36)). Analysis of the reaction products shows that, experimentally, about 68% of the lithium in the alloy pool reacted. This compares favorably to the program results, which show that 64.86% of the lithium would react in an equilibrium system. Thus the program correctly predicts the extent of the reaction. Therefore, one can conclude that the HEDL large scale experiments did not produce an equilibrium interaction, despite the practically instantaneous and complete reaction observed.

#### viii) Conclusion

The program presented here is a very effective and easy to use tool. The program can be applied to any modest sized system with little effort. Although the program may not execute efficiently with systems that contain many trace species, using the

program is a much more simple task than writing an efficient program for the task at hand.



### Nomenclature

$a_{ie}$	- The array of stoichiometric coefficients.
$B_e$	- The mass balanced constrained mass of element e.
$b_e$	- The current mass of element e.
$D_i$	- A factor in the $\delta\phi_i$ equation.
$E_i$	- A factor in the $\delta\phi_i$ equation.
$G$	- The system Gibbs free energy.
$G^{\circ}(T)$	- The Gibbs free energy of species i at 1 atm.
$H$	- The system enthalpy.
$H^{\circ}(298)$	- The enthalpy of species i at 1 atm. and 298K.
$L$	- The system Lagrangian.
$M$	- The number of elements in the system.
$m_i$	- The mass of species i from the previous step.
$N$	- the number of species in the system.
$n_i$	- The current mass of species i.
$p$	- The system pressure.
$p_o$	- Atmospheric pressure.
$S$	- The system entropy.
$T$	- The system temperature.
$V$	- The system volume.
$\Delta G_f^{\circ}(T)$	- The Gibbs free energy of formation at 1 atm.
$\Delta H_f^{\circ}(298)$	- The heat of formation at 1 atm. and 298K.
$\epsilon$	- The mass balance convergence parameter.
$\eta_e$	- A factor for the second Lagrangian multiplier.
$\mu_i$	- The chemical potential of species i.
$\mu_i^{\circ}$	- The chemical potential of species i at 1 atm.

- $\sigma$  - The program step size.
- $\tau$  - The minimum program step size.
- $\phi_i$  - The transformed form of  $n_i$ .
- $\chi_i$  - The first Lagrangian multiplier.
- $\chi_\phi$  - The second Lagrangian multiplier.
- $\omega$  - A factor for the second Lagrangian multiplier.

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### Appendix

This appendix contains the listing of the computer program in three sections. The first section contains the main program listing. The next section contains the subroutine used in the propane/air application. The final section contains the subroutine used in the  $\text{Li}_{17}\text{Pb}_{83}/\text{H}_2\text{O}$  application. The program is written in standard FORTRAN.

```

1 C CHEMQ
2 C***** CHEMQ
3 C CHEMQ
4 C CHEMEQ Program By Jim Herzog 4/86 - 5/86 CHEMQ
5 C CHEMQ
6 C This program evaluates the chemical equilibrium of a heterogeneousCHEMQ
7 C mixture. It assumes that the mixture consists of up to 3 homogeneousCHEMQ
8 C phases ( liquid, solid, and gas ). CHEMQ
9 C The program is based on the first-order steepest descent method of CHEMQ
10 C Van Zeggeren and Storey. The program is similar to the chemical CHEMQ
11 C equilibrium subroutine used in CORCON ( MLTREA subroutine ), but is CHEMQ
12 C more general and less powerful than MLTREA. CHEMQ
13 C This program is designed to work with simple systems; number of CHEMQ
14 C species <= 20, number of elements <= 10, and separated phases. For CHEMQ
15 C the program to work with any system, all one needs to do is to adjustCHEMQ
16 C the CHEMO subroutine and adjust the data file CHEMIN.DAT CHEMQ
17 C CHEMQ
18 C***** CHEMQ
19 C CHEMQ
20 C References: CHEMQ
21 C 1. S. H. Storey and F. Van Zeggeren, 'The Computation of Chemical CHEMQ
22 C Equilibrium Compositions II', Can. Jour. of Chem. Eng., 48, CHEMQ
23 C Oct. 1970), p. 591-593 CHEMQ
24 C 2. F. Van Zeggeren and S. H. Storey, 'The Computation of Chemical CHEMQ
25 C Equilibrium', Cambridge Univ. Press, Cambridge Ma. (1970). CHEMQ
26 C CHEMQ
27 C***** CHEMQ
28 C CHEMQ
29 C Definition of Variables CHEMQ
30 C CHEMQ
31 C Let S denote species; S = 1, NUMSPE CHEMQ
32 C Let E denote elements; E = 1, NUMELE CHEMQ
33 C CHEMQ
34 C Input / Output: CHEMQ
35 C P = Pressure ( N/M**2 ) CHEMQ
36 C T = Temperature ( K ) CHEMQ
37 C XMOL(S) = Number of moles of the species ( MOLE ) CHEMQ
38 C CHEMPO(S) = Chemical potential evaluated at T and 1 atm ( J/MOLE ) CHEMQ
39 C ASC(E,S) = Array of stoichiometric coefficients CHEMQ
40 C PHASE(S) = Phase of the species CHEMQ
41 C DSTEP = Step size CHEMQ
42 C CONVRG = Convergence parameter for minimum step size CHEMQ
43 C EPSILN = Convergence Epsilon for element balance conversion CHEMQ
44 C TRACE = Trace species cutoff parameter CHEMQ
45 C NDEBUB = Debug output parameter CHEMQ
46 C SPLIST(S) = A character list of problem specific species CHEMQ
47 C ELLIST(E) = A character list of problem specific elements CHEMQ
48 C PTITLE = The problem run title CHEMQ
49 C CHEMQ
50 C Internal Arrays: CHEMQ
51 C XINT(S) = Amount of species at start of current step CHEMQ
52 C XBEG(S) = Initial amount of species CHEMQ
53 C CHEMPO(S) = Chemical potential of the species CHEMQ
54 C BELE(E) = Element balances for the problem CHEMQ
55 C BDIF(E) = Difference between the problem element balances and the CHEMQ
56 C current element balance values CHEMQ
57 C BNEW(E) = Updated element balances CHEMQ

```

```

58 C ETA(E)      = 1st Lagrangian multiplier factor      CHEMQ
59 C OMEGA(E)    = 1st Lagrangian multiplier factor      CHEMQ
60 C D(S)        = Factor in the delta phi equation      CHEMQ
61 C E(S)        = Factor in the delta phi equation      CHEMQ
62 C DELPHI(S)   = Delta phi                             CHEMQ
63 C DELPHO(S)   = Delta phi of previous step           CHEMQ
64 C DUMVEC(E)   = Iterative calculational vector        CHEMQ
65 C DUMRAY(E,E) = Iterative calculational array         CHEMQ
66 C XMAX(S)     = The maximum possible amount of each species CHEMQ
67 C XDUM(S)     = A dummy vector used to evaluate XMAX  CHEMQ
68 C                                                     CHEMQ
69 C   Internal Scalars:                                CHEMQ
70 C GNEW        = Updated Gibb's free energy ( J )      CHEMQ
71 C GOLD        = Gibb's free energy of previous iteration CHEMQ
72 C XPHI        = 2nd Lagrangian multiplier             CHEMQ
73 C NUMELE      = The number of elements in the problem CHEMQ
74 C NUMSPE      = The number of species in the problem  CHEMQ
75 C XMOLG       = The moles of gas in the system        CHEMQ
76 C XMOLL       = The moles of liquid in the system     CHEMQ
77 C XMOLS       = The moles of solid in the system      CHEMQ
78 C DSTEPO      = Step size at the beginning of the program CHEMQ
79 C DIREC       = The current direction of the Gibbs free energy surface CHEMQ
80 C                                                     CHEMQ
81 C*****CHEMQ
82 C                                                     CHEMQ
83 C   IMPLICIT DOUBLE PRECISION ( A-H, O-Z )            CHEMQ
84 C   IMPLICIT INTEGER ( I-N )                          CHEMQ
85 C                                                     CHEMQ
86 C   DIMENSION XMOL(20), CHEMPO(20), ASC(10,20), XBEG(20), ETA(10), CHEMQ
87 C   1          XINT(20), CHEMPO(20), BELE(10), BDIF(10), DELPHI(20), CHEMQ
88 C   2          DUMVEC(10), DUMRAY(10,10), OMEGA(10), BNEW(10), D(20), CHEMQ
89 C   3          E(20), DELPHO(20), XMAX(20), XDUM(20)    CHEMQ
90 C                                                     CHEMQ
91 C   CHARACTER*1 PHASE(20)                              CHEMQ
92 C                                                     CHEMQ
93 C   COMMON / PARAM /                                    CHEMQ
94 C   1 DSTEP, CONVRG, EPSILN, TRACE                      CHEMQ
95 C   COMMON / CHEM /                                     CHEMQ
96 C   1 NUMSPE, NUMELE,                                   CHEMQ
97 C   2 PHASE, ASC                                         CHEMQ
98 C                                                     CHEMQ
99 C   IWRITE = 0                                           CHEMQ
100 C   IDEBUG = 11                                          CHEMQ
101 C   EPSMAT = .001                                        CHEMQ
102 C                                                     CHEMQ
103 C-----CHEMQ
104 C   INPUT VARIABLES, GIBB'S FREE ENERGY, AND CHEMICAL POTENTIALS CHEMQ
105 C-----CHEMQ
106 C                                                     CHEMQ
107 C   First we set needed input variables by calling the input subrou- CHEMQ
108 C   ine CHEMIN                                           CHEMQ
109 C   CALL CHEMIN (                                         CHEMQ
110 C   1                                                     CHEMQ
111 C   2                                                     CHEMQ
112 C   3 T, P, XBEG, NDEBEG )                               CHEMQ
113 C                                                     CHEMQ
114 C   DSTEPO = DSTEP                                       CHEMQ

```

```

115      IF ( NDEBUG .EQ. 1 ) OPEN ( 11, FILE = 'DEBUG.DAT', STATUS =
116      1      'NEW' )
117      C
118      C      Next we call the subroutine CHEMO, which gives the temperature
119      C      dependant variables CHEMP0(S)
120      CALL CHEMO (
121      1      T,
122      2
123      3      CHEMP0 )
124      C
125      C      Next we evaluate the starting values of the Gibb's free energy
126      C      and the chemical potential of the species by calling subroutine GIBBS
127      CALL GIBBS (
128      1      T, P, XBEG, CHEMP0,
129      2
130      3      GOLD, CHEMP0 )
131      C
132      C-----
133      C      ELEMENT ABUNDANCES, INITIAL SPECIES COMPOSITIONS AND SPECIES MAX.
134      C-----
135      C
136      C      The element abundances are set by mass balance constraints and
137      C      must be held constant throughout the search for the equilibrium
138      C      condition
139      DO 100 J = 1, NUMELE
140      BELE(J) = 0.
141      DO 105 I = 1, NUMSPE
142      BELE(J) = BELE(J) + ASC(J,I) * XBEG(I)
143      105 CONTINUE
144      100 CONTINUE
145      C
146      DO 150 I = 1, NUMSPE
147      XINT(I) = XBEG(I)
148      150 CONTINUE
149      C
150      DO 160 I = 1, NUMSPE
151      XMAX(I) = 1.D30
152      DO 170 J = 1, NUMELE
153      XDUM(I) = ASC(J,I) / BELE(J)
154      IF ( XDUM(I) .EQ. 0. ) GO TO 180
155      XMAX(I) = DMIN1( XMAX(I), XDUM(I) )
156      180 CONTINUE
157      170 CONTINUE
158      160 CONTINUE
159      C
160      C***** DEBUG DATA *****
161      IF ( NDEBUG .EQ. 1 ) THEN
162      WRITE (IDEBU,190)
163      190      FORMAT ( ' BELE ' )
164      WRITE (IDEBU,372) ( BELE(J), J = 1, NUMELE )
165      WRITE (IDEBU,191)
166      191      FORMAT ( ' XMAX ' )
167      WRITE (IDEBU,462) ( XMAX(I), I = 1, NUMSPE )
168      END IF
169      C*****
170      C
171      NINT = 0

```

```

172 C
173 C-----CHEMQ
174 C BEGINNING OF THE MAIN CALCULATIONAL LOOP CHEMQ
175 C-----CHEMQ
176 C CHEMQ
177 1000 CONTINUE CHEMQ
178 C CHEMQ
179 C First we calculate the difference between the current element bal- CHEMQ
180 C ances and the constrained balances CHEMQ
181 DO 200 J = 1, NUMELE CHEMQ
182 BDIF(J) = BELE(J) CHEMQ
183 DO 205 I = 1, NUMSPE CHEMQ
184 BDIF(J) = BDIF(J) - ASC(J,I) * XINT(I) CHEMQ
185 205 CONTINUE CHEMQ
186 200 CONTINUE CHEMQ
187 C CHEMQ
188 C Now we print intermediate values to the screen CHEMQ
189 IF ( DBLE( NINT / 10 ) .EQ. DBLE( NINT ) / 10. ) THEN CHEMQ
190 WRITE (IWRITE,215) NINT, GOLD CHEMQ
191 WRITE (IWRITE,216) CHEMQ
192 WRITE (IWRITE,462) ( XINT(I), I = 1, NUMSPE ) CHEMQ
193 END IF CHEMQ
194 C CHEMQ
195 C***** DEBUG DATA ***** CHEMQ
196 IF ( NDEBUG .EQ. 1 ) THEN CHEMQ
197 WRITE (IDEBUG,215) NINT, GOLD CHEMQ
198 215 FORMAT ( ' -----' / CHEMQ
199 1 ' ITERATION # = ', I5, ' G = ', 1P1611.4 ) CHEMQ
200 WRITE (IDEBUG,217) CHEMQ
201 217 FORMAT ( ' CHEMPO' ) CHEMQ
202 WRITE (IDEBUG,462) ( CHEMPO(I), I = 1, NUMSPE ) CHEMQ
203 WRITE (IDEBUG,216) CHEMQ
204 216 FORMAT ( ' XINT ' ) CHEMQ
205 WRITE (IDEBUG,462) ( XINT(I), I = 1, NUMSPE ) CHEMQ
206 WRITE (IDEBUG,220) CHEMQ
207 220 FORMAT ( ' BDIF ' ) CHEMQ
208 WRITE (IDEBUG,372) ( BDIF(J), J = 1, NUMELE ) CHEMQ
209 END IF CHEMQ
210 C***** CHEMQ
211 C CHEMQ
212 C-----CHEMQ
213 C SET UP AND SOLVE EQUATIONS FOR LAGRANGIAN MULTIPLIERS CHEMQ
214 C-----CHEMQ
215 C CHEMQ
216 C Set up array on left hand side of equations CHEMQ
217 DO 300 J = 1, NUMELE CHEMQ
218 DO 310 L = J, NUMELE CHEMQ
219 SUM = 0. CHEMQ
220 DO 320 I = 1, NUMSPE CHEMQ
221 SUM = SUM + ASC(J,I) * ASC(L,I) * XINT(I) * XINT(I) CHEMQ
222 320 CONTINUE CHEMQ
223 DUMRAY(J,L) = SUM CHEMQ
224 DUMRAY(L,J) = SUM CHEMQ
225 310 CONTINUE CHEMQ
226 300 CONTINUE CHEMQ
227 C CHEMQ
228 C Set up vector on right hand side of eta equation CHEMQ

```



```

229      DO 350 J = 1, NUMELE                                CHEMQ
230          SUM = 0.                                          CHEMQ
231      DO 360 I = 1, NUMSPE                                CHEMQ
232          SUM = SUM + ASC(J,I) * CHEMPD(I) * XINT(I) * XINT(I) CHEMQ
233 360      CONTINUE                                          CHEMQ
234          DUMVEC(J) = SUM                                   CHEMQ
235 350      CONTINUE                                          CHEMQ
236      C                                                    CHEMQ
237      C***** DEBUG DATA *****                          CHEMQ
238          IF ( NDEBUG.EQ. 1 ) THEN                         CHEMQ
239              WRITE (IDEBUG,370)                             CHEMQ
240 370          FORMAT ( ' INTERMEDIATE ARRAY ' )              CHEMQ
241              DO 371 J = 1, NUMELE                           CHEMQ
242                  WRITE (IDEBUG,372) ( DUMRAY(J,L), L = 1, NUMELE ) CHEMQ
243 371          CONTINUE                                       CHEMQ
244                  WRITE (IDEBUG,373)                         CHEMQ
245 373          FORMAT ( 10X, ' INTERMEDIATE VECTOR ' )       CHEMQ
246                  WRITE (IDEBUG,372) ( DUMVEC(J), J = 1, NUMELE ) CHEMQ
247 372          FORMAT ( 5X, 1P5G11.4 / 6X, 1P5G11.4 )        CHEMQ
248              END IF                                         CHEMQ
249      C*****                                                    CHEMQ
250      C                                                    CHEMQ
251      C      Now to solve for the inverse of the intermediate array DUMRAY CHEMQ
252      C by calling the math subroutine MATINV               CHEMQ
253          CALL MATINV (                                       CHEMQ
254              1  NUMELE, EPSMAT, IWRITE,                     CHEMQ
255              2  DUMRAY,                                       CHEMQ
256              3  DETER )                                       CHEMQ
257      C                                                    CHEMQ
258      C
259      C***** DEBUG DATA *****                          CHEMQ
260          IF ( NDEBUG.EQ. 1 ) THEN                         CHEMQ
261              WRITE (IDEBUG,375)                             CHEMQ
262 375          FORMAT ( ' INTERMEDIATE ARRAY DETERMINANT ' ) CHEMQ
263              WRITE (IDEBUG,*) DETER                         CHEMQ
264              WRITE (IDEBUG,376)                             CHEMQ
265 376          FORMAT ( ' INTERMEDIATE ARRAY INVERSE ' )     CHEMQ
266              DO 377 J = 1, NUMELE                           CHEMQ
267                  WRITE (IDEBUG,372) ( DUMRAY(J,L), L = 1, NUMELE ) CHEMQ
268 377          CONTINUE                                       CHEMQ
269              END IF                                         CHEMQ
270      C*****                                                    CHEMQ
271      C                                                    CHEMQ
272      C      We can now solve for the additive factors in the first Lagrangian CHEMQ
273      C multiplier ( ETA(NUMELE) and OMEGA(NUMELE) )        CHEMQ
274          DO 380 I = 1, NUMELE                               CHEMQ
275              ETA(I) = 0.                                     CHEMQ
276              OMEGA(I) = 0.                                   CHEMQ
277              DO 381 J = 1, NUMELE                           CHEMQ
278                  ETA(I) = ETA(I) + DUMRAY(I,J) * DUMVEC(J) CHEMQ
279                  OMEGA(I) = OMEGA(I) - DUMRAY(I,J) * BDIF(J) CHEMQ
280 381          CONTINUE                                       CHEMQ
281 380          CONTINUE                                       CHEMQ
282      C                                                    CHEMQ
283      C***** DEBUG DATA *****                          CHEMQ
284          IF ( NDEBUG.EQ. 1 ) THEN                         CHEMQ
285              WRITE (IDEBUG,390)                             CHEMQ

```

```

286 390      FORMAT ( ' ETA ' )
287      WRITE (IDEBU,372) ( ETA(J), J = 1, NUMELE )
288      WRITE (IDEBU,391)
289 391      FORMAT ( ' OMEGA ' )
290      WRITE (IDEBU,372) ( OMEGA(J), J = 1, NUMELE )
291      END IF
292 C*****
293 C
294 C-----
295 C      FIND THE FACTORS D AND E
296 C-----
297 C
298      DO 400 I = 1, NUMSPE
299          E(I) = 0.
300          SUM = 0.
301          DO 410 J = 1, NUMELE
302              SUM = SUM + ETA(J) * ASC(J,I)
303              E(I) = E(I) + OMEGA(J) * ASC(J,I) * XINT(I)
304 410      CONTINUE
305          D(I) = XINT(I) * ( CHEMPQ(I) - SUM )
306 400      CONTINUE
307 C
308 C***** DEBUG DATA *****
309      IF ( NDEBU .EQ. 1 ) THEN
310          WRITE (IDEBU,415)
311 415      FORMAT ( ' D ' )
312          WRITE (IDEBU,462) ( D(I), I = 1, NUMSPE )
313          WRITE (IDEBU,416)
314 416      FORMAT ( ' E ' )
315          WRITE (IDEBU,462) ( E(I), I = 1, NUMSPE )
316      END IF
317 C*****
318 C
319 C-----
320 C      SET UP AND SOLVE FOR 2ND LAGRANGIAN MULTIPLIER
321 C-----
322 C
323 C      First we calculate the the summation terms in the equation
324      SUMD = 0.
325      SUME = 0.
326      DO 420 I = 1, NUMSPE
327          SUMD = SUMD + D(I) * D(I)
328          SUME = SUME + E(I) * E(I)
329 420      CONTINUE
330 C
331 C      Now we can calculate the 2nd Lagrangian multiplier. We must make
332 C      sure that DSTEP**2 <= SUME, if it isn't, we adjust the step size
333 2000      CONTINUE
334          IF ( ( DSTEP * DSTEP ) .LE. SUME ) THEN
335              DSTEP = 1.5 * DSTEP
336 C***** DEBUG DATA *****
337          IF ( NDEBU .EQ. 1 ) THEN
338              WRITE (IDEBU,430) DSTEP
339 430          FORMAT ( ' DSTEP IS TOO SMALL - NEW DSTEP = ', 1P1611.4 )
340          END IF
341 C*****
342          GO TO 2000

```

```

343         END IF                                CHEMQ
344 C                                             CHEMQ
345         XPHI = -1. * DSQRT( SUMD / ( DSTEP * DSTEP - SUME ) ) CHEMQ
346 C                                             CHEMQ
347 C-----CHEMQ
348 C     CALCULATE DELPHI                        CHEMQ
349 C-----CHEMQ
350         DO 450 I = 1, NUMSPE                    CHEMQ
351             DELPHI(I) = ( D(I) / XPHI ) - E(I)    CHEMQ
352 450     CONTINUE                                CHEMQ
353 C                                             CHEMQ
354 C***** DEBUG DATA *****                  CHEMQ
355         IF ( NDEBUG .EQ. 1 ) THEN                CHEMQ
356             WRITE (IDEBUG,460) XPHI                CHEMQ
357 460         FORMAT ( ' XPHI = ', 1P1611.4 )        CHEMQ
358             WRITE (IDEBUG,461)                    CHEMQ
359 461         FORMAT ( ' DELPHI ' )                  CHEMQ
360             WRITE (IDEBUG,462) ( DELPHI(I), I = 1, NUMSPE ) CHEMQ
361 462         FORMAT ( 5X, 1P5611.4 / 6X, 1P5611.4 / 7X, 1P5611.4 / CHEMQ
362             1                                     8X, 1P5611.4 ) CHEMQ
363         END IF                                CHEMQ
364 C*****CHEMQ
365 C                                             CHEMQ
366 C-----CHEMQ
367 C     CALCULATE XMOL AND GNEW                  CHEMQ
368 C-----CHEMQ
369 C                                             CHEMQ
370         DO 500 I = 1, NUMSPE                    CHEMQ
371             XMOL(I) = XINT(I) * DEXP( DELPHI(I) ) CHEMQ
372 500     CONTINUE                                CHEMQ
373 C                                             CHEMQ
374 C     Find the new Gibbs free energy and the chemical potential CHEMQ
375         CALL GIBBS (                             CHEMQ
376             1   T, P, XMOL, CHEMP0,                CHEMQ
377             2                                     CHEMQ
378             3   GNEW, CHEMP0 )                      CHEMQ
379 C                                             CHEMQ
380 C-----CHEMQ
381 C     CHECK CONVERGENCE CONDITIONS              CHEMQ
382 C-----CHEMQ
383 C                                             CHEMQ
384 C     First we evaluate the new element balances CHEMQ
385         DO 510 J = 1, NUMELE                      CHEMQ
386             BNEW(J) = 0.                            CHEMQ
387             DO 515 I = 1, NUMSPE                    CHEMQ
388                 BNEW(J) = BNEW(J) + ASC(J,I) * XMOL(I) CHEMQ
389 515     CONTINUE                                CHEMQ
390 510     CONTINUE                                CHEMQ
391 C                                             CHEMQ
392 C     Now we check to see if the new element abundances have converged CHEMQ
393 C to the element abundances set by mass balance constraints CHEMQ
394         IBCHCK = 0                                CHEMQ
395         DO 520 J = 1, NUMELE                      CHEMQ
396             BCHECK = DABS( BELE(J) - BNEW(J) ) / BELE(J) CHEMQ
397             IF ( BCHECK .GT. EPSILN ) IBCHCK = 1    CHEMQ
398 520     CONTINUE                                CHEMQ
399 C                                             CHEMQ

```

```

400 C      Now we check to see if the step size has converged to the desired CHEM0
401 C      minimum value CHEM0
402      ISCHCK = 0 CHEM0
403      IF ( DSTEP .GT. CONVRG ) ISCHCK = 1 CHEM0
404 C CHEM0
405 C      If both IBCHCK and ISCHCK equal 0, then the minimum Gibbs free CHEM0
406 C      energy has been found. CHEM0
407      IF ( ( IBCHCK .EQ. 0 ) .AND. ( ISCHCK .EQ. 0 ) ) GO TO 9000 CHEM0
408 C CHEM0
409 C-----CHEM0
410 C      ELIMINATE TRACE SPECIES CHEM0
411 C-----CHEM0
412 C CHEM0
413      DO 550 I = 1, NUMSPE CHEM0
414      IF ( XMOL(I) .LT. ( TRACE * XMAX(I) ) ) XMOL(I) = 0. CHEM0
415 550 CONTINUE CHEM0
416 C CHEM0
417 C-----CHEM0
418 C      ADJUST STEP SIZE CHEM0
419 C-----CHEM0
420 C CHEM0
421 C      First we determine the direction the program is traveling along CHEM0
422 C      the Gibbs free energy surface ( and a measure of the surface steep- CHEM0
423 C      ness ). The step size is then adjusted accordingly. CHEM0
424      IF ( NINT .EQ. 0 ) THEN CHEM0
425      DSTEP = .5 * DSTEP CHEM0
426      ELSE CHEM0
427      SUM = 0. CHEM0
428      DO 600 I = 1, NUMSPE CHEM0
429      SUM = SUM + DELPHI(I) * DELPHO(I) CHEM0
430 600 CONTINUE CHEM0
431      DIREC = SUM / ( DSTEP * DSTEP ) CHEM0
432      IF ( DIREC .LT. 0. ) DSTEP = .5 * DSTEP CHEM0
433      IF ( DIREC .GT. .7 ) DSTEP = DMIN1( DSTEP0, 2.*DSTEP ) CHEM0
434      END IF CHEM0
435 C CHEM0
436 C-----CHEM0
437 C      RESET LOOP VARIABLES CHEM0
438 C-----CHEM0
439 C CHEM0
440      DO 700 I = 1, NUMSPE CHEM0
441      XINT(I) = XMOL(I) CHEM0
442      DELPHO(I) = DELPHI(I) CHEM0
443 700 CONTINUE CHEM0
444 C CHEM0
445      GOLD = GNEW CHEM0
446      NINT = NINT + 1 CHEM0
447 C CHEM0
448 C      We now return to the beginning of the loop CHEM0
449      GO TO 1000 CHEM0
450 C CHEM0
451 C-----CHEM0
452 C      MINIMUM GIBBS FREE ENERGY FOUND! CHEM0
453 C-----CHEM0
454 C CHEM0
455 9000 CONTINUE CHEM0
456 C CHEM0

```

```

457 C      We have found the minimum Gibb's free energy and can now call the CHEM0
458 C      output subroutine (CHOUT) CHEM0
459 C      CALL CHOUT ( CHEM0
460 C      1 T, P, XBEG, GNEW, XMOL, BELE, NINT CHEM0
461 C      2 CHEM0
462 C      3 ) CHEM0
463 C CHEM0
464 C      That's all folks! CHEM0
465 C      END CHEM0
466 C CHEM0
467 C***** CHIN
468 C CHIN
469 C      SUBROUTINE CHEMIN ( CHIN
470 C      1 CHIN
471 C      2 CHIN
472 C      3 T, P, XMOL, NDEBUG ) CHIN
473 C CHIN
474 C      This subroutine is the user interface that sets the input CHIN
475 C      variables used in the main program CHEM0 CHIN
476 C      IMPLICIT DOUBLE PRECISION ( A-H, O-Z ) CHIN
477 C      IMPLICIT INTEGER ( I-N ) CHIN
478 C CHIN
479 C      DIMENSION XMOL(20), ASC(10,20) CHIN
480 C CHIN
481 C      CHARACTER*1 PHASE(20), CPARAM, CDEBUG CHIN
482 C      CHARACTER*10 SPLIST(20), ELLIST(10) CHIN
483 C      CHARACTER*12 DATFIL CHIN
484 C      CHARACTER*80 PTITLE CHIN
485 C CHIN
486 C      COMMON / PARAM / CHIN
487 C      1 DSTEP, CONVRG, EPSILN, TRACE CHIN
488 C      COMMON / CHEM / CHIN
489 C      1 NUMSPE, NUMELE, CHIN
490 C      2 PHASE, ASC CHIN
491 C      COMMON / PRLST / CHIN
492 C      1 SPLIST, ELLIST, PTITLE CHIN
493 C CHIN
494 C      IWRITE = 0 CHIN
495 C      IREAD = 0 CHIN
496 C      IDATA = 12 CHIN
497 C CHIN
498 C----- CHIN
499 C      READ IN PROBLEM SPECIFIC DATA FROM SPECIFIED DATA FILE CHIN
500 C----- CHIN
501 C CHIN
502 C      We must first ask the user to specify the name of the input data CHIN
503 C      file CHIN
504 C      WRITE (IWRITE,5) CHIN
505 C      5 FORMAT ( 5X, ' Enter the name of the input data file [', CHIN
506 C      1 'filename.ext]') CHIN
507 C      READ (IREAD,6) DATFIL CHIN
508 C      6 FORMAT ( 12A ) CHIN
509 C      OPEN ( IDATA, FILE = DATFIL ) CHIN
510 C CHIN
511 C      First we read in the number of species and elements CHIN
512 C      READ (IDATA,*) NUMSPE, NUMELE CHIN
513 C CHIN

```

```

514 C      Now we read in the character lists SPLIST and ELLIST      CHIN
515      DO 10 I = 1, NUMSPE      CHIN
516          READ (IDATA,11) SPLIST(I)      CHIN
517      11      FORMAT (10A)      CHIN
518      10      CONTINUE      CHIN
519 C      CHIN
520      DO 15 J = 1, NUMELE      CHIN
521          READ (IDATA,11) ELLIST(J)      CHIN
522      15      CONTINUE      CHIN
523 C      CHIN
524 C      Lastly, we read in the stoichiometric coefficient array ASC      CHIN
525      DO 20 J = 1, NUMELE      CHIN
526          READ (IDATA,*) ( ASC(J,I), I = 1, NUMSPE )      CHIN
527      20      CONTINUE      CHIN
528 C      CHIN
529 C-----CHIN
530 C      PROMPT THE USER FOR PROBLEM PARAMETERS      CHIN
531 C-----CHIN
532 C      CHIN
533 C      First we prompt the user for the main problem variables; the      CHIN
534 C      system temperature and pressure, and the initial species mass      CHIN
535          WRITE (IWRITE,100)      CHIN
536      100      FORMAT ( ' Enter the problem title, up to 80 characters ' )      CHIN
537          READ (IREAD,105) PTITLE      CHIN
538      105      FORMAT ( 80A )      CHIN
539 C      CHIN
540          WRITE (IWRITE,110)      CHIN
541      110      FORMAT ( 5X, ' Enter the system temperature [K] and the system', CHIN
542      1      ' pressure [N/M**2] ' )      CHIN
543          READ (IREAD,*) T, P      CHIN
544 C      CHIN
545          WRITE (IWRITE,115)      CHIN
546      115      FORMAT ( 5X, ' Enter the initial mass [MOLE] of ' )      CHIN
547          DO 120 I = 1, NUMSPE      CHIN
548              WRITE (IWRITE,125) I, SPLIST(I)      CHIN
549      125      FORMAT ( ' species number', I3, ': ', 10A )      CHIN
550              READ (IREAD,*) XMOL(I)      CHIN
551      120      CONTINUE      CHIN
552 C      CHIN
553 C      Lastly, we prompt the user to change the problem parameters if he      CHIN
554 C      wants to, and ask him if he wants debug output      CHIN
555          DSTEP = 2.5      CHIN
556          CONVRG = 1.D-4      CHIN
557          EPSILN = 1.D-4      CHIN
558          TRACE = 1.D-5      CHIN
559          WRITE (IWRITE,200) DSTEP, CONVRG, EPSILN, TRACE      CHIN
560      200      FORMAT ( ' The initial value of the step size = ',      CHIN
561      1          1P1611.4 /      CHIN
562      2          ' The step size convergence parameter = ',      CHIN
563      3          1P1611.4 /      CHIN
564      4          ' The mass balance convergence parameter = ',      CHIN
565      5          1P1611.4 /      CHIN
566      6          ' The trace species cutoff parameter = ',      CHIN
567      7          1P1611.4 /      CHIN
568      8          5X, ' Do you want to change these parameters',      CHIN
569      9          ' [y/n] ? ' )      CHIN
570          READ (IREAD,210) CPARAM      CHIN

```

```

571 210  FORMAT ( A )                                CHIN
572      IF ( ( CPARAM.EQ. 'Y' ) .OR. ( CPARAM.EQ. 'y' ) ) THEN  CHIN
573      WRITE (IWRITE,220)                            CHIN
574 220  FORMAT ( ' Enter the new initial step size ' )    CHIN
575      READ (IREAD,*) DELLAM                          CHIN
576      WRITE (IWRITE,221)                            CHIN
577 221  FORMAT ( ' Enter the new step size convergence parameter ' ) CHIN
578      READ (IREAD,*) CONVRG                          CHIN
579      WRITE (IWRITE,222)                            CHIN
580 222  FORMAT ( ' Enter the new mass balance convergence',  CHIN
581      1      ' parameter ' )                        CHIN
582      READ (IREAD,*) EPSILN                          CHIN
583      WRITE (IWRITE,223)                            CHIN
584 223  FORMAT ( ' Enter the new trace species cutoff parameter ' ) CHIN
585      READ (IREAD,*) TRACE                          CHIN
586      END IF                                         CHIN
587 C                                                CHIN
588      WRITE (IWRITE,230)                            CHIN
589 230  FORMAT ( ' Do you want debug output [y/n] ? ' )  CHIN
590      READ (IREAD,210) CDEBUG                        CHIN
591      IF ( ( CDEBUG.EQ. 'Y' ) .OR. ( CDEBUG.EQ. 'y' ) ) THEN CHIN
592      NDEBUG = 1                                     CHIN
593      ELSE                                           CHIN
594      NDEBUG = 0                                     CHIN
595      END IF                                         CHIN
596 C                                                CHIN
597 C      That's all folks!                            CHIN
598      RETURN                                         CHIN
599      END                                           CHIN
600 C                                                CHIN
601 C*****GIBBS*****GIBBS
602 C                                                GIBBS
603      SUBROUTINE GIBBS (                               GIBBS
604      1 T, P, XMOL, CHEMP0,                           GIBBS
605      2                                                GIBBS
606      3 G, CHEMP0 )                                   GIBBS
607 C                                                GIBBS
608 C      This subroutine evaluates the Gibb's free energy and the chemical GIBBS
609 C potential of the species                           GIBBS
610      IMPLICIT DOUBLE PRECISION ( A-H, O-Z )          GIBBS
611      IMPLICIT INTEGER ( I-N )                       GIBBS
612 C                                                GIBBS
613      DIMENSION XMOL(20), CHEMP0(20), CHEMP0(20), ASC(10,20) GIBBS
614 C                                                GIBBS
615      CHARACTER*1 PHASE(20)                          GIBBS
616 C                                                GIBBS
617      COMMON / CHEM /                                GIBBS
618      1 NUMSPE, NUMELE,                               GIBBS
619      2 PHASE, ASC                                     GIBBS
620 C                                                GIBBS
621 C      First we evaluate XMOLG, XMOLL, and XMOLS      GIBBS
622      XMOLG = 0.                                       GIBBS
623      XMOLL = 0.                                       GIBBS
624      XMOLS = 0.                                       GIBBS
625      DO 100 I = 1, NUMSPE                            GIBBS
626      IF ( PHASE(I).EQ. 'G' ) XMOLG = XMOLG + XMOL(I) GIBBS
627      IF ( PHASE(I).EQ. 'L' ) XMOLL = XMOLL + XMOL(I) GIBBS

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```

628      IF ( PHASE(I) .EQ. 'S' ) XMOLS = XMOLS + XMOL(I)      GIBBS
629 100 CONTINUE      GIBBS
630 C      GIBBS
631 C      Now we can evaluate G and CHEMPO      GIBBS
632      G = 0.      GIBBS
633      RT = 8.3143 * T      GIBBS
634      DO 110 I = 1, NUMSPE      GIBBS
635          IF ( XMOL(I) .EQ. 0. ) THEN      GIBBS
636              CHEMPO(I) = CHEMPO(I)      GIBBS
637          ELSE      GIBBS
638              IF ( PHASE(I) .EQ. 'G' ) CHEMPO(I) = CHEMPO(I) + RT *      GIBBS
639 1          DLOG( ( P * XMOL(I) ) / ( 1.013D5 * XMOLG ) )      GIBBS
640              IF ( PHASE(I) .EQ. 'L' ) CHEMPO(I) = CHEMPO(I) + RT *      GIBBS
641 1          DLOG( XMOL(I) / XMOLL )      GIBBS
642              IF ( PHASE(I) .EQ. 'S' ) CHEMPO(I) = CHEMPO(I) + RT *      GIBBS
643 1          DLOG( XMOL(I) / XMOLS )      GIBBS
644          END IF      GIBBS
645 C      GIBBS
646      G = G + CHEMPO(I) * XMOL(I)      GIBBS
647 110 CONTINUE      GIBBS
648 C      GIBBS
649 C      That's all folks!      GIBBS
650      RETURN      GIBBS
651      END      GIBBS
652 C      GIBBS
653 C***** CHOUT
654 C      CHOUT
655      SUBROUTINE CHOUT (      CHOUT
656 1 T, P, XBEG, G, XMOL, BELE, NINT      CHOUT
657 2      CHOUT
658 3 )      CHOUT
659 C      CHOUT
660 C      This subroutine writes the initial species mass, system tempera-      CHOUT
661 C      ture, system pressure, equilibrium species mass, and the minimum      CHOUT
662 C      Gibb's free energy      CHOUT
663      IMPLICIT DOUBLE PRECISION ( A-H, O-Z )      CHOUT
664      IMPLICIT INTEGER ( I-N )      CHOUT
665 C      CHOUT
666      DIMENSION XMOL(20), XBEG(20), ASC(10,20), BELE(10)      CHOUT
667 C      CHOUT
668      CHARACTER*10 SPLIST(20), ELLIST(10)      CHOUT
669      CHARACTER*1 PHASE(20)      CHOUT
670      CHARACTER*80 PTITLE      CHOUT
671 C      CHOUT
672      COMMON / CHEM /      CHOUT
673 1 NUMSPE, NUMELE,      CHOUT
674 2 PHASE, ASC      CHOUT
675      COMMON / PRLST /      CHOUT
676 1 SPLIST, ELLIST, PTITLE      CHOUT
677 C      CHOUT
678      OPEN ( 11, FILE = 'CHEMOUT.DAT', STATUS = 'NEW' )      CHOUT
679 C      CHOUT
680      IOUT = 11      CHOUT
681 C      CHOUT
682      WRITE (IOUT,10) PTITLE      CHOUT
683 10      FORMAT ( 80A / / )      CHOUT
684 C      CHOUT

```



```

685      WRITE (IOUT,100) T, P, G, NINT                                CHOUT
686 100   FORMAT ( 5X, ' For T = ', 1P1611.4, ' K and P = ',      CHOUT
687      1      1P1611.4, ' Pa ' / 5X, ' The minimum Gibbs free',  CHOUT
688      2      ' energy = ', 1P1611.4, ' J ' / 5X, ' The number of', CHOUT
689      3      ' iterations = ', I6 )                                CHOUT
690 C                                           CHOUT
691      WRITE (IOUT,102)                                              CHOUT
692 102   FORMAT (// 15X, '-----' )                                CHOUT
693      WRITE (IOUT,105)                                              CHOUT
694 105   FORMAT ( 15X, '! Element ! Element mass [MOLE]!' /      CHOUT
695      1      15X, '!-----!-----!' )                          CHOUT
696      DO 106 I = 1, NUMELE                                          CHOUT
697      WRITE (IOUT,107) ELLIST(I), BELE(I)                          CHOUT
698 107   FORMAT ( 15X, '!', 2X, A10, '!', 5X, 1P1615.6, '!' )    CHOUT
699 106   CONTINUE                                                    CHOUT
700      WRITE (IOUT,108)                                              CHOUT
701 108   FORMAT ( 15X, '-----' )                                CHOUT
702 C                                           CHOUT
703      WRITE (IOUT,109)                                              CHOUT
704 109   FORMAT(//15X,'-----',CHOUT
705      1      '-----' )                                           CHOUT
706      WRITE (IOUT,110)                                              CHOUT
707 110   FORMAT ( 15X,'! Species ! Initial mass [MOLE] ! Equilibrium',CHOUT
708      1      ' mass [MOLE]!' )                                     CHOUT
709      WRITE (IOUT,111)                                              CHOUT
710 111   FORMAT ( 15X,'!-----!-----!-----',CHOUT
711      1      '-----!' )                                           CHOUT
712      DO 200 I = 1, NUMSPE                                          CHOUT
713      WRITE (IOUT,201) SPLIST(I), XBEG(I), XMOL(I)                CHOUT
714 201   FORMAT ( 15X, '!', 2X, A10, '!', 5X, 1P1615.6, 1X, '!',  CHOUT
715      1      8X, 1P1615.6, 1X, '!' )                                CHOUT
716 200   CONTINUE                                                    CHOUT
717      WRITE (IOUT,250)                                              CHOUT
718 250   FORMAT ( 15X,'-----',CHOUT
719      1      '-----' )                                           CHOUT
720 C                                           CHOUT
721 C      That's all folks!                                          CHOUT
722      RETURN                                                         CHOUT
723      END                                                            CHOUT
724 C                                           CHOUT
725 C*****
726 C
727      SUBROUTINE MATINV (
728      1 N, EPS, IW,
729      2 A,
730      3 FDETER )
731 C
732 C Subroutine MATINV computes the determinant and the inverse
733 C matrix by Gauss-Jordan elimination using maximal pivoting.
734 C
735 C N----- NUMBER OF MATRIX EQUATIONS [A] (X) = (B)
736 C          CURRENT MAXIMUM IS 50
737 C EPS----- CHECK VALUE FOR NEAR SINGULARITY OF PIVOT ELEMENT
738 C A----- 'LEFT' HAND 2D MATRIX
739 C FDETER---- DETERMINANT
740 C IW----- UNIT NUMBER FOR ERROR MESSAGE OUTPUT
741 C

```

```
742 C Taken from Carnahan, Luther, Wilkes p.290 by J. J. Barry
743 C
744 C DOUBLE PRECISION REAL*8 (USING 8087 ARITHMETIC)
745 C
746 C IMPLICIT DOUBLE PRECISION ( A-H, O-Z )
747 C IMPLICIT INTEGER ( I-M )
748 C
749 C DIMENSION IROW(50),JCOL(50),JORD(50),Y(50)
750 C DIMENSION A(10,10),B(10)
751 C
752 C Error report if exceed allowable dimensions.
753 C
754 C IF (N .LE. 50) GO TO 5
755 C WRITE (IW,301)
756 301 FORMAT(' ERROR IN MATINV - exceeded maximum dimension')
757 C FDETER = 0.
758 C RETURN
759 C
760 C Begin elimination procedure.
761 C
762 C 5 DETER = 1.
763 C DO 18 K=1,N
764 C KM1 = K - 1
765 C
766 C Search for pivot element.
767 C
768 C PIVOT = 0.
769 C DO 11 I=1,N
770 C DO 11 J=1,N
771 C
772 C Scan IROW and JCOL arrays for invalid pivot subscripts.
773 C
774 C IF (K .EQ. 1) GO TO 9
775 C DO 8 ISCAN=1,KM1
776 C DO 8 JSCAN=1,KM1
777 C IF (I .EQ. IROW(ISCAN)) GO TO 11
778 C IF (J .EQ. JCOL(JSCAN)) GO TO 11
779 8 CONTINUE
780 9 IF (DABS(A(I,J)) .LE. DABS(PIVOT)) GO TO 11
781 C PIVOT = A(I,J)
782 C IROW(K) = I
783 C JCOL(K) = J
784 11 CONTINUE
785 C
786 C Insure that selected pivot is larger than eps.
787 C
788 C IF (DABS(PIVOT) .GT. EPS) GO TO 13
789 C FDETER = 0.
790 C RETURN
791 C
792 C Update the determinant value.
793 C
794 13 IROWK = IROW(K)
795 C JCOLK = JCOL(K)
796 C DETER = DETER * PIVOT
797 C
798 C Normalize pivot row elements.
```

```
799 C
800     DO 14 J=1,N
801         A(IROWK,J) = A(IROWK,J)/PIVOT
802     14 CONTINUE
803 C
804 C Carry out elimination and develop inverse.
805 C
806     A(IROWK,JCOLK) = 1./PIVOT
807     DO 18 I=1,N
808         AIJCK = A(I,JCOLK)
809         IF (I .EQ. IROWK) GOTO 18
810         A(I,JCOLK) = -AIJCK/PIVOT
811         DO 17 J=1,N
812             IF (J .NE. JCOLK) A(I,J) = A(I,J) - AIJCK*A(IROWK,J)
813     17 CONTINUE
814     18 CONTINUE
815 C
816 C Order solution values (if any) and create JORD array.
817 C
818     DO 20 I=1,N
819         IROWI = IROW(I)
820         JCOLI = JCOL(I)
821         JORD(IROWI) = JCOLI
822     20 CONTINUE
823 C
824 C Adjust sign of determinant.
825 C
826     INTCH = 0
827     NM1 = N - 1
828     DO 22 I=1,NM1
829         IP1 = I + 1
830         DO 22 J = IP1,N
831             IF (JORD(J) .GE. JORD(I)) GOTO 22
832             JTEMP = JORD(J)
833             JORD(J) = JORD(I)
834             JORD(I) = JTEMP
835             INTCH = INTCH + 1
836     22 CONTINUE
837     IF ((INTCH/2)*2 .NE. INTCH) DETER = -DETER
838 C
839 C Unscramble the inverse.
840 C - first by rows
841 C
842     26 DO 28 J=1,N
843         DO 27 I=1,N
844             IROWI = IROW(I)
845             JCOLI = JCOL(I)
846             Y(JCOLI) = A(IROWI,J)
847     27 CONTINUE
848     DO 28 I=1,N
849         A(I,J) = Y(I)
850     28 CONTINUE
851 C
852 C Then by columns.
853 C
854     DO 30 I=1,N
855         DO 29 J=1,N
```

```
856          IROWJ = IROW(J)
857          JCOLJ = JCOL(J)
858          Y(IROWJ) = A(I,JCOLJ)
859      29      CONTINUE
860          DO 30 J=1,N
861              A(I,J) = Y(J)
862      30      CONTINUE
863      C
864          FDETER = DETER
865          RETURN
866          END
```

```

1      SUBROUTINE CHERO (                                CHERO
2      1 T,                                              CHERO
3      2                                              CHERO
4      3 CHERO )                                         CHERO
5 C                                                     CHERO
6 C   This subroutine calculates the chemical potential and the phase CHERO
7 C   of the species specified in this application. Where necessary, the CHERO
8 C   the chemical potential data from the JANAF tables has been curve CHERO
9 C   fitted to give CHERO(T) formulas. Only temperatures between 600K CHERO
10 C   and 1400K are valid                                CHERO
11      IMPLICIT DOUBLE PRECISION ( A-H, O-Z )          CHERO
12      IMPLICIT INTEGER ( I-N )                        CHERO
13 C                                                     CHERO
14      DIMENSION ASC(10,20), CHERO(20), GHSTAN(20), HDF(20) CHERO
15 C                                                     CHERO
16      CHARACTER*1 PHASE(20)                           CHERO
17 C                                                     CHERO
18      COMMON / CHERO /                                CHERO
19      1 NUMSPE, NUMELE,                                CHERO
20      2 PHASE, ASC                                      CHERO
21 C                                                     CHERO
22 C   This subroutine uses the alternate definition of the standard CHERO
23 C   chemical potential.                                CHERO
24 C   CHERO = ( GIBBSO - HSTAND ) + HDF                  CHERO
25 C   where, GIBBSO = Gibb's free energy at 1atm and T   CHERO
26 C   HSTAND = enthalpy at 1atm and T                   CHERO
27 C   HDF = heat of formation at 1atm and 298K          CHERO
28 C                                                     CHERO
29 C   defining GHSTAN = ( GIBBSO - HSTAND ) / T, this subroutine CHERO
30 C   evaluates GHSTAN(T) for a given T and thus CHERO(T). This data is CHERO
31 C   drawn from the JANAF tables.                      CHERO
32 C                                                     CHERO
33 C   Species 1: Li                                     CHERO
34      GHSTAN(1) = -22.347 - .033 * T + 6.0758D-6 * T * T CHERO
35      HDF(1) = 2.381D3                                  CHERO
36      PHASE(1) = 'L'                                    CHERO
37 C                                                     CHERO
38 C   Species 2: Pb                                     CHERO
39      GHSTAN(2) = -59.831 - .03266 * T + 5.8283D-6 * T * T CHERO
40      HDF(2) = 4.289D3                                  CHERO
41      PHASE(2) = 'L'                                    CHERO
42 C                                                     CHERO
43 C   Species 3: Li17Pb83                              CHERO
44 C   The properties of this species are extrapolated from the properties CHERO
45 C   of Li and Pb                                     CHERO
46      GHSTAN(3) = .17 * GHSTAN(1) + .83 * GHSTAN(2)    CHERO
47      HDF(3) = -7.83D3                                  CHERO
48      PHASE(3) = 'L'                                    CHERO
49 C                                                     CHERO
50 C   Species 4: H2                                     CHERO
51      GHSTAN(4) = -119.44 - .03121 * T + 5.23D-6 * T * T CHERO
52      HDF(4) = 0.                                        CHERO
53      PHASE(4) = 'G'                                    CHERO
54 C                                                     CHERO
55 C   Species 5: H2O                                     CHERO
56      GHSTAN(5) = -175.66 - 3.5924D-2 * T + 4.962D-6 * T * T CHERO
57      HDF(5) = -2.4183D5                               CHERO

```



```
1  $STORAGE:2
2  $NOFLOATCALLS
3      SUBROUTINE CHEMO ( T, CHEMP0 )
4      IMPLICIT DOUBLE PRECISION ( A-H, O-Z )
5      IMPLICIT INTEGER ( I-N )
6      DIMENSION ASC(10,20), CHEMP0(20)
7      CHARACTER*1 PHASE(20)
8      COMMON / CHEM / NUMSPE, NUNELE, PHASE, ASC
9  C
10 C   CO2
11      CHEMP0(1) = -3.96409D5
12      PHASE(1) = 'G'
13 C
14 C   N2
15      CHEMP0(2) = 0.
16      PHASE(2) = 'G'
17 C
18 C   H2O
19      CHEMP0(3) = -1.23934D5
20      PHASE(3) = 'G'
21 C
22 C   CO
23      CHEMP0(4) = -3.026496D5
24      PHASE(4) = 'G'
25 C
26 C   H2
27      CHEMP0(5) = 0.
28      PHASE(5) = 'G'
29 C
30 C   H
31      CHEMP0(6) = 9.480526D4
32      PHASE(6) = 'G'
33 C
34 C   HO
35      CHEMP0(7) = 6.953808D3
36      PHASE(7) = 'G'
37 C
38 C   O
39      CHEMP0(8) = 1.0829865D5
40      PHASE(8) = 'G'
41 C
42 C   NO
43      CHEMP0(9) = 6.251314D4
44      PHASE(9) = 'G'
45 C
46 C   O2
47      CHEMP0(10) = 0.
48      PHASE(10) = 'G'
49 C
50 C   C
51      CHEMP0(11) = 0.
52      PHASE(11) = 'S'
53 C
54      RETURN
55      END
```