

Theoretical Energy Required Per SWU

- From thermodynamics

$$\frac{\text{kWh}}{\text{SWU}} = \frac{4RT}{M(1-\alpha)^2}$$

$$R = \text{Gas Constant} = 8.31441 \frac{\text{J}}{\text{mole } ^\circ\text{K}}$$

Where, $T = ^\circ\text{K}$

$M = \text{Molecular Mass}$

if $T = 58^\circ\text{C}$,

$$\text{min Energy/SWU} = 702 \frac{\text{kWh}}{\text{SWU}}$$

actually, $\approx 3000 \frac{\text{kWh}}{\text{SWU}}$

History

US Capacity in mid 1970's 17,000,000 SWU/y

Cascade Improvement & 10,000,000 $\frac{\text{SWU}}{\text{y}}$
Cascade Upgrading Prog (1983)

total 27,000,000 $\frac{\text{SWU}}{\text{y}}$

Because of plant cancellations in 1970's and 1980's, and because of European built plants,

there is considerable excess capacity

Figure 2.21

Centrifuge Method

<u>Date</u>	<u>Events</u>
1938	<i>JW Beam, Germany in WWII</i>
1950's	<i>Germans built larger gas centrifuges</i>
1960's	<i>Centrifuges become competitive</i>
1970	<i>FRG and Netherlands build a plant</i>
1976	<i>Japanese build a plant</i>
1977	<i>Carter Administration announces that the next enrichment plant would use the gas centrifuge process.</i>
1985	<i>Almost completed gas centrifuge plant (8,800,000 SWU/y) shut down by Reagan administration for laser isotope plant.</i>

Principles

- A rotating drum compresses gas molecules in the cylinder to outer wall**
- Lighter molecules concentrate in the center**

Figure 3.7

Gas Centrifuge factor;

$$\alpha = 1 + \left\{ \frac{[M_H - M_L] \omega^2 a^2}{2RT} \right\}$$

where; ω = angular velocity (rad/s)

a = radius of rotor (inside dimension)

M_H = Molecular Wt. of $^{38}\text{UF}_6$

M_L = Molecular Wt. of $^{35}\text{UF}_6$

for 30 cm diameter rotor at $350 \frac{\text{m}}{\text{s}}$ @ 300°K

$\alpha = 1.1$ to 1.2 (Compare to gas diffusion)

Features

- **Small capacities; a $9,000,000 \frac{\text{SWU}}{\text{y}}$ plant requires 90,000 to 100,000 machines**
- **Reliability - if mean time between failure is 3 years, then more than 3 machines break per h**
- **Lower Power requirements $\approx 300 \frac{\text{kWh}}{\text{SWU}}$
if 1 kWh $\approx 5\text{¢}$, then;
Gas centrifuge cost $\approx \frac{\$15}{\text{SWU}}$**

Gaseous Diffusion $\approx \frac{\$ 150}{\text{SWU}}$
Nozzle Method

- **Developed by Becker in FRG, 1960**
(later in South Africa, Netherlands)
- **UF₆ (5%) + H₂ (95%) @ 20 -200 torr forced**
into orifice (See figure 3.8)
 $\alpha = 1.015$
- **Must be very precise and clean ($\approx 30\mu$)**
- **Smaller number of stages than gaseous**
diffusion to get to 3% (500 vs 1200)
- **Slightly higher electricity consumption**
 $4000 \frac{\text{kWh}}{\text{SWU}}$

Atomic Vapor Laser Isotope Separation
(AVLIS)

- **First demonstrated in 1975**
- **Principle relies on many absorption lines in**
U (300,000)
- **There is a significant separation between**
³⁵U and ³⁸U which can be exploited by the
use of variable wavelength lasers.

Figure 3.9

Figure 3.10

- 1.) Pool of liquid U formed
- 2.) Photo excite ^{35}U at 5915\AA
- 3.) Use UV light to ionize excited atom
- 4.) Collect positively charged ^{35}U

Advantage - $300 \frac{\text{kWh}}{\text{SWU}}$

plus less moving parts and higher reliability

Overall Costs For Enriched U

$$PE = \frac{(PU + PC)F}{P} + PS \sum S$$

Price of Enriched U	Price of Natural U	Conversion Costs	SWU Costs
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The price of enriched U can be optimized with respect to waste tails

$$\frac{\delta PE}{\delta x_w} = 0$$

gives;

$$\frac{PU + PC}{PS} = \frac{(x_f - x_w) \sum (1 - 2x_w)}{x_w (1 - x_w)} + (1 - 2x_f) \ln \left[\frac{x_w (1 - x_f)}{x_w (1 - x_w)} \right]$$

Problem -2

Calculate the cost of enriched U (in $\frac{\$}{\text{kg}}$) if the product is 2.8% enriched, the tails assay is 0.25%, and the conversion loss is 0.5%. Assume the price of natural U is \$40/kg, the cost of conversion is \$6/kg, and the price is \$80/SWU.

Answer:

$$\frac{F}{P} = \frac{(2.8-0.25)}{(0.7111-0.25)} = 5.531$$

$$V(x_f) = (2 \cdot 0.00711 - 1) \cdot \ln\left[\frac{0.00711}{(1-0.00711)}\right] \\ = 4.869$$

$$V(x_p) = (2 \cdot 0.028 - 1) \cdot \ln\left[\frac{0.028}{(1-0.028)}\right] = 3.348$$

$$V(x_w) = (2 \cdot 0.0025 - 1) \cdot \ln\left[\frac{0.0025}{(1-0.0025)}\right] = 5.959$$

$$S = 3.348 + 4.531 \cdot 5.959 - 5.531 \cdot 4.869 = 3.418 \frac{\text{SWU}}{\text{kg}}$$

$$PE = \left[\frac{40}{(1-0.005)} + 6\right] \cdot 5.531 + 80 \cdot 3.418 = \$ 529/\text{kg}$$

Total Fabricated Costs

$$FF = \left\{ \left[\frac{PU}{(1 - l_f) \Sigma(1 - l_c)} \right] + \frac{PC}{(1 - l_f)} \right\} \frac{F}{P} + \frac{PS}{(1 - l_f)} \Sigma S + PF$$

l_c = fraction of U lost in conversion

l_f = fraction of U lost in fabrication

PF = Price of Fabricated Fuel

Problem -3

What is the cost of fabricated fuel if the price for fabrication is \$200/kg and there is an 0.8% loss during fabrication. Use the numbers from problem 2 for nat. U, conversion, and enrichments costs.

$$FF = \left\{ \left[\frac{40}{(1 - 0.005) \Sigma(1 - 0.008)} \right] + \frac{6}{(1 - 0.008)} \right\} \Sigma 5.531$$
$$+ \frac{80}{(1 - 0.008)} \Sigma 3.418 + 200$$

$$FF = 732 \text{ \$/kg}$$

Important Points About the Nuclear Fuel Cycle

- Only 10% of U. S. Uranium requirements are met from domestic sources, 90% comes from outside the U. S. (85% from Canada)
- Imported Russian HEU could provide 40% US in future
- **Worldwide Demand for Enrichment-1996 MSWU/Year**
 - **US-11.2**
 - **Eastern Europe-4.3**
 - **Western Europe-12.0**
 - **Far East-6.2**
 - **Other-0.4**
 - **Total ≈ 34**

Facility	Countries Involved	SWU/y Capacity (12/31/95)	% of World Market (1994?)	Technology Used
U. S. Enrichment Corp.	U.S.	19.3	≈40 (70% of US)	Gaseous Diffusion
Eurodif	France, Belgium, Spain, Italy	10.8	≈20	Gaseous Diffusion
ChinaNucl. Energy Ind. Corp.	Peoples Rep. of China	0.5	NA	Gaseous Diffusion
Minatom	Russia	14	≈30	Gas Centrifuge
Urenco	Netherlands, Germany, U. K.	3.4	≈10	Gas Centrifuge
Power Reactor & Nuclear Fuel Dev. Corp.	Japan	0.2	NA	Gas Centrifuge
Japan Nuclear Fuel Industries Company	Japan	0.6	NA	Gas Centrifuge
Atomic Energy Commission	South Africa	0.3	NA	NA
		total-48.7		