

**What is Currently Being Used in Fission Power Plants Today?**

**Fuel Element Performance**

**Fuel**

**Cladding**

**Zircalloy**

**Enrichment**

**Metallic Fuel**

- **Early U Fuels**
- **LMR Fuels**

**Oxide Fuel**

- **Fuel Chemistry**
- **Fission Product Behaviour**
  - Swelling**
  - Fission Gas Release**
- **Pore Migration and Restructuring**

# Metallic Fuels

- During first 10 years of fission reactor research almost all fuels were metallic.
- Now ( see last lecture) practically all power reactor fuels are oxides.
- Need fissionable isotope  $U^{235}$ ,

$$t_{\frac{1}{2}} = 710 \text{ million years}$$

## *Uranium*

### Phases

$\alpha$  = orthorhombic----- $a \neq b \neq c$

$\beta$  = tetragonal ----- $a = b \neq c$

$\gamma$  = body centered cubic-- $a = b = c$   
(figure)

Anisotropy of Alpha Uranium Phase		
Lattice Direction	Å	Thermal Expansion Coefficient °C <sup>-1</sup> x 10 <sup>-6</sup> (25-125)
100	2.852	21.17
010	5.685	-1.15
001	4.945	23.2
		Volume 45.8

# **Dimensional Stability**

## **1.) Irradiation Growth**

**Change of shape without appreciable volume change**

## **2.) Irradiation Creep**

**Change of shape under an external stress**

## **3.) Swelling**

**No change of shape but a change in volume**

***Plus two other phenomena NOT related to irradiation !***

## **A.) Thermal Ratcheting**

**Thermal cycling of polycrystal textured specimen in  $\alpha$  phase**

## **B.) Surface Roughing**

**Cycling through the  $\alpha$ - $\beta$  phase transition**

## Necessary Definitions

**Problem:** *What unit to use in describing radiation damage in fissile material?*

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**Properties are more related to fission events than to neutron fluence**

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**No single definition satisfactory!**

A.) Reactor Designer - More concerned with power density than fission density

B.) Reactor Physicist- More concerned with percentage of fissile atoms lost by all processes than with % fissioned

C.) Material Scientists- Can't agree!  
i.e., a 70% burnup of U atoms in UO<sub>2</sub> -Steel cermet means more than  
 $3 \times 10^{21}$  fissions/cm<sup>3</sup>

**Deposit  
in fuel**

**Total  
Energy  
Release**

**MWd**

**t**

**?** **?**

**ton**

**tonne**

**total  
fuel ?**

**Just  
U ?**

**Energy  
per <sup>235</sup>U  
Fission**

169 MeV - FP  
5 MeV - n  
5 MeV -  $\gamma$

12 MeV - FP  
Decay

8 MeV -  $\beta, \gamma$   
Decay

-----  
199 MeV

+ 10-12 neutrinos

**Instantaneous**

**Design Dependent**

## Another Unit Which is Misinterpreted -

$$\frac{\text{Fission}}{\text{cm}^3}$$

- Necessary for heat transfer calculations

• What is included in  $\text{cm}^{-3}$  ?

*Normally it is not the cladding or the coating on the fuel pellets*

$$\frac{\text{Fission}}{\text{cm}^3} = (\text{frac. of U atoms fissioned}) \cdot (\text{density of U in fuel})$$

$$= \frac{N_f}{N_U} \cdot \{nvt\sigma_f\} \cdot \frac{\rho N_A}{m'}$$

where;

$$\frac{N_f}{N_U} = \text{fraction of U atoms that can fission}$$

$\rho$  = fuel density

$m'$  = M. Wt. of fuel / # of U atoms in molecule

$N_A$  = Avogadro's Number

## Relate Burn -up and Integral Flux

Let  $N$  = atoms of fissile isotopes

$\sigma_c, \sigma_f$  = capture and fission  
xsections, respectively

$$\frac{dN}{dt} = -Nnv\sigma_a$$

where  $\sigma_a = \sigma_c + \sigma_f$

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*Integrating and finding the % of fissile atoms lost, one finds;*

$$100 \left\{ \frac{(N_o - N)}{N_o} \right\} = 100 \left\{ 1 - e^{-nvt\sigma_a} \right\}$$

*The % of atoms fissioned is then;*

$$100 \left[ \frac{\sigma_f}{\sigma_a} \right] \left\{ 1 - e^{-nvt\sigma_a} \right\}$$

*when  $nvt\sigma_a \ll 1$ ,  $\exp(-x) \approx 1-x$ ,*

$$\% \text{ atoms fissioned} = 100 nvt\sigma_f$$

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*since  $\sigma_f \approx 550$  barns for  $^{35}\text{U}$  in thermal flux;*

$$\% \text{ B.U. of } ^{35}\text{U} \text{ atoms} = 55000 \text{ b} \cdot (nvt)$$

*If only a fraction of U atoms are fissionable;*

$$\frac{N_f}{N_U} \left[ 100 \cdot nvt\sigma_f \right]$$

## ***Example***

- Assume 1 fission = 200 MeV

$$200 \cdot 10^6 \frac{\text{eV}}{\text{fission}} \cdot 1.6 \cdot 10^{-19} \frac{\text{watt} \cdot \text{s}}{\text{eV}} \cdot \frac{1 \text{day}}{86,400 \text{s}}$$
$$= 3.7 \cdot 10^{-16} \frac{\text{watt} \cdot \text{d}}{\text{fission}}$$

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$$\frac{\text{watt} \cdot \text{d}}{g_{\text{fuel}}} = 3.7 \cdot 10^{-16} \cdot \left( \frac{1}{\rho_{\text{fuel}}} \right) \cdot \left( \frac{\text{fissions}}{\text{cm}^3} \right)$$

$$\text{or, } \frac{\text{MWd}}{\text{tonne} \cdot U} = 3.7 \cdot 10^{-16} \cdot \left( \frac{1}{\rho_{\text{fuel}}} \right) \cdot \left( \frac{\text{fissions}}{\text{cm}^3} \right) \cdot \frac{m'}{A}$$

where  $A$  = atomic wt. of  $U$

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***What if not all of the energy released is captured by the fuel?***

- can only count on 169 MeV K.E. of FP's  
Plus 12 MeV Decay of FP's

$$\frac{\text{MWd}}{\text{tonne} \cdot \text{fuel}} = 1.85 \cdot 10^{-18} \cdot \left( \frac{1}{\rho_{\text{fuel}}} \right) \cdot \left( \frac{\text{fissions}}{\text{cm}^3} \right) \cdot E_f$$

where  $E_f$  is the fission energy (MeV) deposited in the fuel



**Another way to express this is:**

$$\frac{\text{MWd - in - fuel}}{\text{tonne - U}} = 1.85 \cdot 10^{-18} \cdot \left( \frac{E_f}{\rho_{\text{fuel}}} \right) \cdot \left( \frac{\text{fissions}}{\text{cm}^3} \right) \cdot \frac{m}{A}$$

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## **What Have We Forgotten?**

**1.) Conversion of fertile to fissile**

( important at low enrichments and at high burn up)

**2.) Fast fission**

Few % in thermal reactors

**3.) Absorption of gamma rays**

From the parent fuel rod or from surrounding fuel rods

$$\frac{\text{MWd} \cdot \text{within} \cdot \text{fuel}}{\text{tonne} \cdot \text{fuel}} = \frac{A}{m'} \cdot \left( - \right)$$

$$\frac{\text{MWd within fuel}}{\text{tonne U}} = 1.85 \cdot 10^{-18} \frac{m' E_f}{\rho A} \cdot -$$

$$\frac{\text{fissions}}{\text{cm}^3} = 6.02 \cdot 10^{21} \cdot \left( \frac{\rho N_t}{m' N_U} \right) \cdot \left( - \right)$$

$$\% \cdot \text{of} \cdot \text{all} \cdot \text{atoms} \cdot \text{fissioned} = \frac{N_U}{N_t} \cdot \left( - \right)$$

$$\% \cdot \text{of} \cdot \text{all} \cdot \text{U} \cdot \text{atoms} \cdot \text{fissioned} = 100 \frac{N_f \sigma_f}{N_U} \cdot \left( - \right)$$

$$\text{neutron} \cdot \text{fluence} = nvt$$