

# **Nuclear Issues and Analysis for ARIES Spherical and Advanced Tokamaks**

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# Objectives

- Address key nuclear issues for Spherical and Advanced tokamaks:
  - Protection of center post
  - Breeding capability of blanket options
  - Lifetime of structural components

- Assess impact of nuclear parameters on design choices:

## Parameters

TBR

Mn

Radiation damage

## Issues

Breeder type

Blanket thickness/composition

Li enrichment

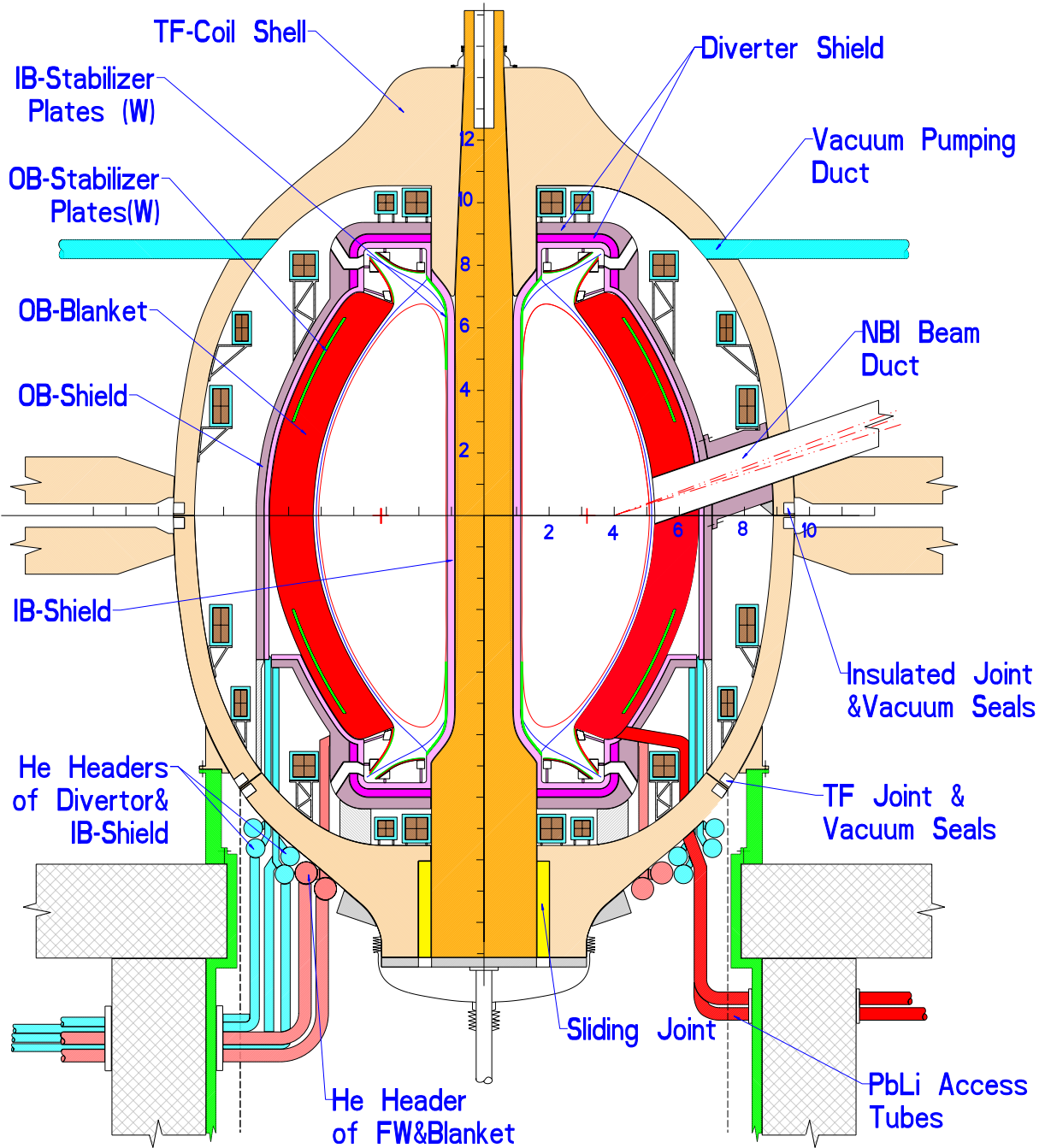
HT and LT components

Service lifetime

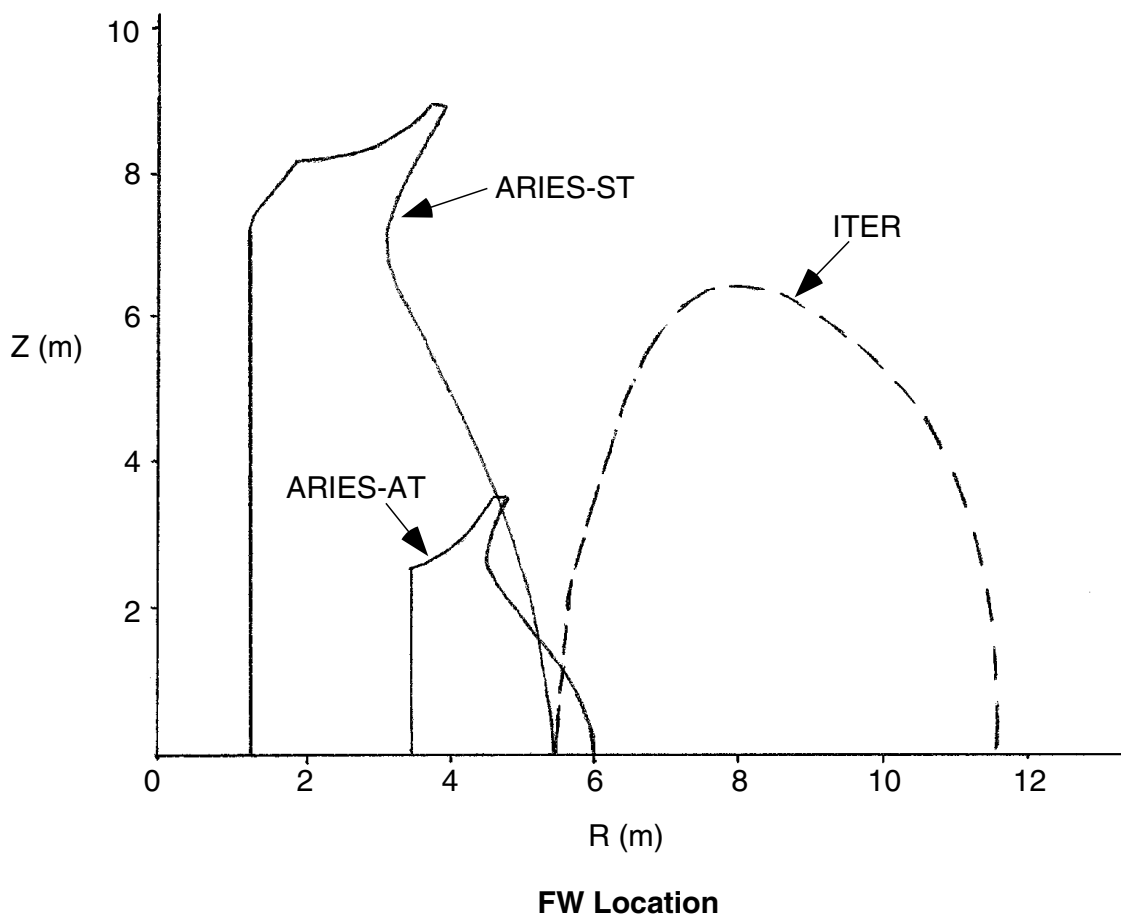
Radial build

- Shielding assessment:
  - Requirements
  - Need for IB shield to protect center post
  - Optimal shield design
- Comparison between 1-D and 3-D neutronics results

## Elevation View of ARIES-ST Power Core



Elevation View of ARIES-ST



First Wall Location

# Tritium Breeding Requirement

- **3-D overall TBR should be 1.1**  
10% breeding margin accounts for:
  - Uncertainties in Xn data of Li and Pb ( 7%)
  - Uncertainties in calculations and modeling ( 2%)
  - T losses [hold-ups and decay] (< 1%)
  - T supply for new power plants (< 1%)
- **Actual net TBR after plant operation may range between 1.01 and 1.2**
- **Blanket design should be flexible to adjust net TBR to 1.01**
- **In case of overbreeding** (net TBR > 1.01), reduce TBR by:
  - Lowering enrichment
  - Replacing back cell(s) by steel shield
- **In case of underbreeding** (net TBR < 1.01), major changes will be needed to adjust TBR:
  - Increase enrichment to 90%
  - Thicken blanket
  - Install blanket on inboard ( $\Rightarrow$  higher P )
  - Add Be to Cell 1 of LiPb blanket (safety!)
  - Reduce A of ARIES-ST (economics !)
  - Change blanket design ( $\Rightarrow$  exclude water from CP)

# ARIES-ST Blanket Neutronics



- Four blanket options proposed for ARIES-ST:
  - LiPb/FS/SiC/He
  - Li/V
  - Li<sub>2</sub>TiO<sub>3</sub>/FS/SiC
  - Li<sub>2</sub>O/SiC

## LiPb/FS/SiC/He is preferred option:

- Compatible with water-cooled center post
- Withstand high wall loadings
- Avoid safety problems associated with other options

- FW/blanket main features:
  - 3.1 cm thick FW (25% FS, 75% He)
  - 1 m thick outboard-only blanket (76% LiPb, 6% FS, 6% He, 12% SiC)
  - 60% enriched Li<sup>6</sup>

- 3-D results:

Overall TBR	1.1
Overall Mn	1.1

- Energy recovered from all components except water-cooled CP

## Peak Radiation Damage to FW per Unit Wall Loading



	<u>ARIES-ST</u>		<u>ARIES-AT</u>	
	<u>1-D</u>	<u>3-D</u>	<u>1-D</u>	<u>3-D</u>
<u>Inboard:</u>				
dpa/FPY	25	13	28	15
He appm/FPY	210	120	1730	1200
H appm/FPY	830	510	1220	480
Nuclear Heating (W/cm <sup>3</sup> )	16	7	12	6
<u>Outboard:</u>				
dpa/FPY	15	11	18	11
⇒ FW/B EOL Fluence (MWy/m <sup>2</sup> )		18		
He appm/FPY	170	110	1410	870
H appm/FPY	660	470	990	350
⇒ FW/B EOL Fluence (MWy/m <sup>2</sup> )				18.5
Nuclear Heating (W/cm <sup>3</sup> )	10	6	9	5

- 1-D model overestimates FW damage and underestimates damage to back components
- 3-D results should be used to re-normalize 1-D n source for individual components

# Differences Between 3-D and 1-D Analyses



	<u>3-D</u>	<u>1-D</u>
Model	actual	toroidal cylindrical
Angular distribution of incident 14 MeV n's on FW	mostly perpendicular ⇒ lower front damage higher back damage	perpendicular and tangential components
Plasma shape	actual	cylindrical
n source distribution	actual	uniform, shifted outward
Reflection from i/b, o/b, div.	actual	no div. effect
Vertical variation of n wall loading	non-uniform ⇒ less reflection from parts off midplane	uniform ⇒ more reflection
Cross section data	pointwise	multi-group



# Subsystem Requirements for Inboard Shield of ARIES-ST

- **Design requirements:** Shield Size
  - Protect CP against radiation for  $> 3$  FPY  
(Cu embrittlement, resistivity change, activation, coolant radiolysis)
  - Enhance outboard breeding
  - Reduce heat load and thermal stress to CP
- **Safety requirements:**
  - Compatible with CP and blanket
- **Economic requirements:**
  - Prolong CP lifetime  
(replacement cost, availability, radwaste stream)
  - Maximize Mn ( $\Rightarrow$  recover i/b heating)
  - Reduce Joule losses ( $\Rightarrow$  minimize shield size)

Unshielded CP does not offer attractive design

Inboard shield competes with CP for valuable space

Contradicting requirements mean inboard shield design is a compromise between several constraints

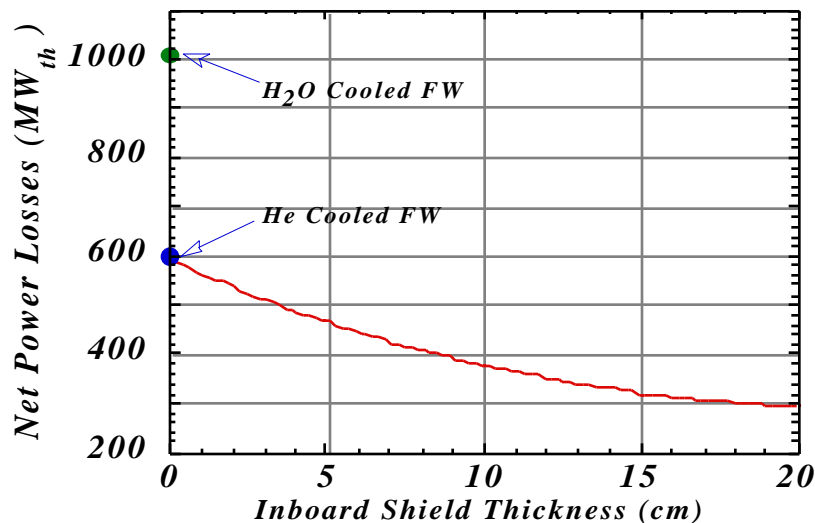
Shielding parameters should be chosen to optimize overall design, not only to minimize Joule losses in CP

# 20 cm Thick He-Cooled Inboard Shield is Optimal for ARIES-ST

- Inboard power losses (and thus COE) minimize near 20 cm thick shield
- Net i/b power losses (in  $MW_{th}$ )=

$$P / \eta + NH_{CP} + PP / \eta - [(SH + NH)_{FW/shld} + 0.9 PP]$$

where  $P$  is CP Joule losses,  
 $\eta$  is thermal conversion efficiency,  
 $SH$  is Surface Heating,  
 $NH$  is Nuclear Heating,  
 $PP$  is He Pumping Power (90% of  $PP$  is recovered as thermal heat)



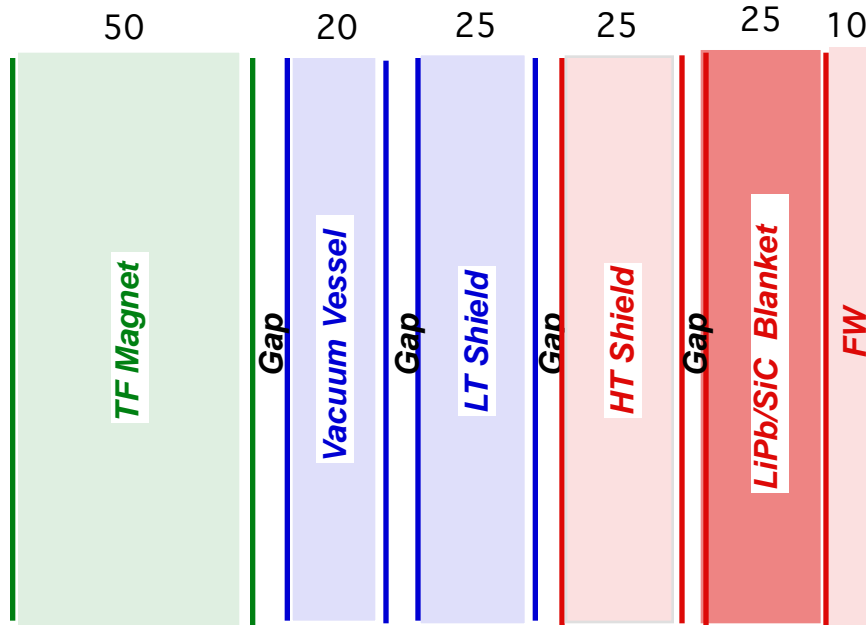
- Designs with i/b shields thinner than 20 cm will have higher COE, lower breeding, higher CP damage, shorter CP lifetime, higher Cu radwaste stream, and higher CP decay heat

# Key Design Parameters



	<u>ARIES-ST</u>	<u>ARIES-AT</u>
Fusion Power (MW)	3000	2200
Net Electric Power (MW <sub>e</sub> )	1000	1000
Aspect ratio	1.6	4
Elongation	3.4	1.9
Major radius (m)	3.2	4.8
Minor radius (m)	2	1.2
Neutron wall loading (MW/m <sup>2</sup> )		
Peak outboard	6.4	6.6
Peak inboard	3.7	5.1
Structural material	FS	SiC/SiC
Radiation damage limit	200 dpa	3% burnup
Plant lifetime (FPY)	40	40

# ARIES-AT Inboard Radial Build

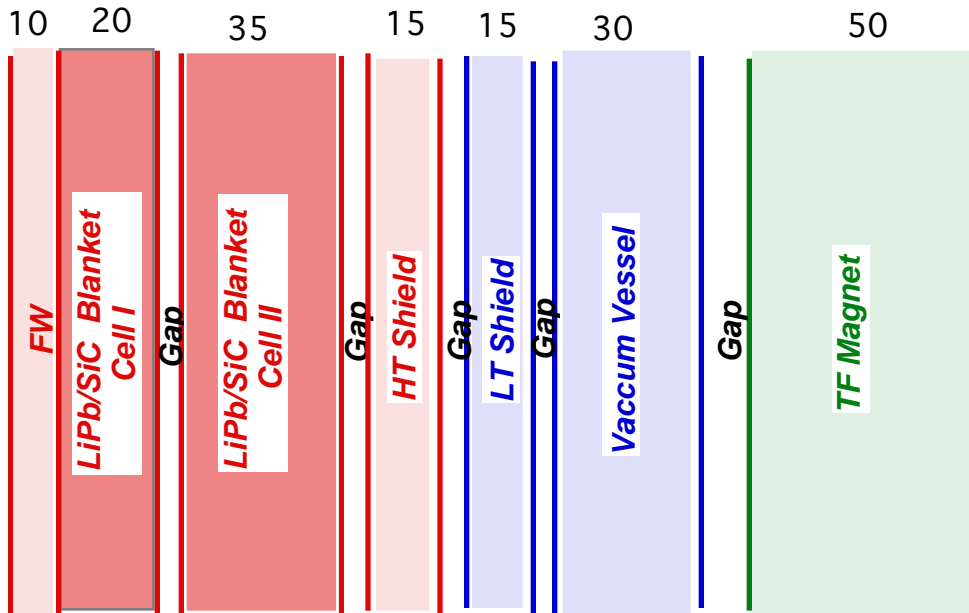


## Components

## Composition

FW	17% SiC , 26% LiPb, 57% void
Blanket	8% SiC , 92% LiPb
HT Shield	15% SiC, 10% LiPb , 75% B-FS
LT Shield	15% FS , 5% H <sub>2</sub> O , 80% WC
Vacuum Vessel	35% FS , 40% H <sub>2</sub> O , 25% WC

# ARIES-AT Outboard Radial Build



## Components

## Composition

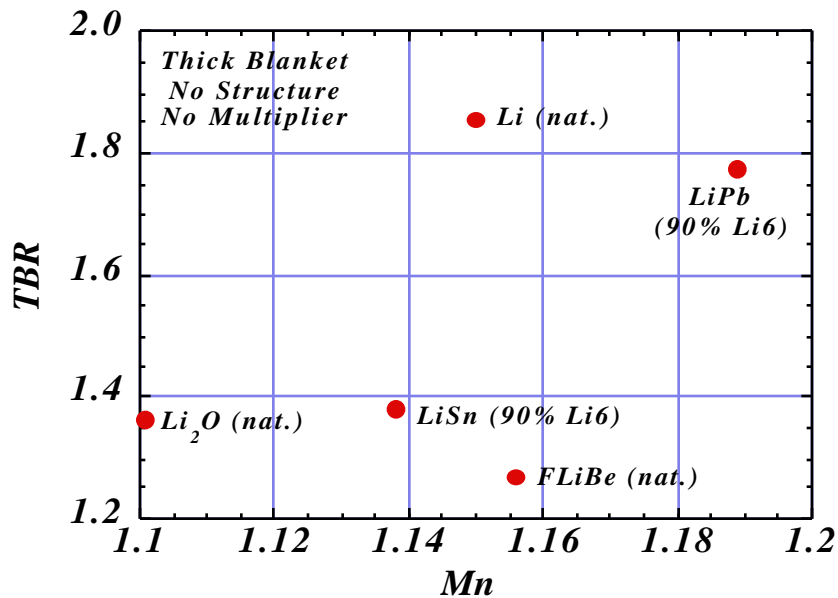
FW	17% SiC , 26% LiPb, 57% void
Blanket	8% SiC , 92% LiPb
HT Shield	15% SiC, 10% LiPb , 75% B-FS
LT Shield	15% FS , 5% H <sub>2</sub> O , 80% B-FS
Vacuum Vessel	25% FS , 60% H <sub>2</sub> O, 15% B-FS

# ARIES-AT Blanket Neutronics

- Three candidate breeders:

-  $\text{Li}_{17}\text{Pb}_{83}$       -  $\text{Li}_{25}\text{Sn}_{75}$       -  $\text{F}_4\text{Li}_2\text{Be}$

*T - M Plot*



- $\text{Li}_{25}\text{Sn}_{75}$  and  $\text{F}_4\text{Li}_2\text{Be}$  have lower breeding potential than  $\text{Li}_{17}\text{Pb}_{83}$
- Other enrichments yield lower TBR
- Structure, penetrations, and geometry degrade overall TBR to 1.1 or less

# ARIES-AT Blanket Neutronics (cont.)



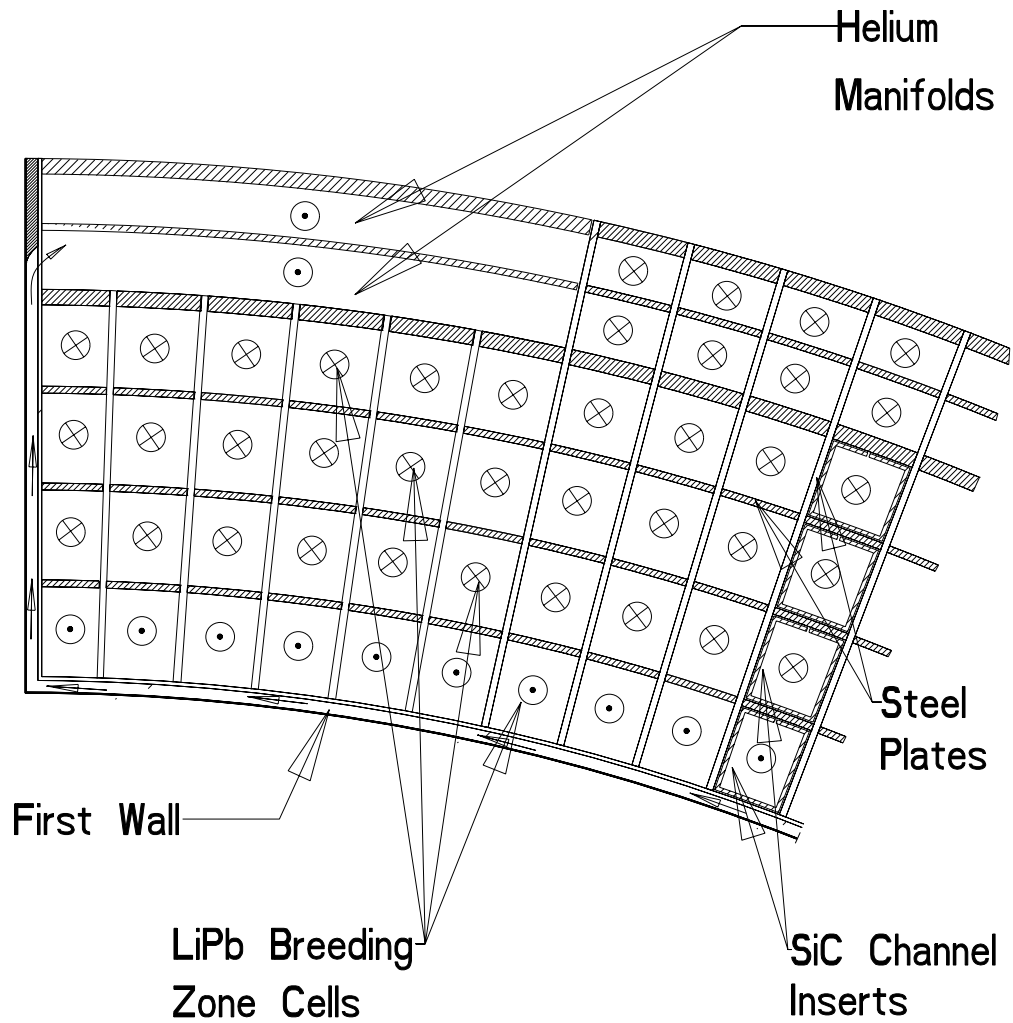
- Actual designs:

	<u>LiPb/SiC</u>	<u>LiSn/SiC</u>	<u>FLiBe/SiC</u>
<b>Overall TBR</b>	<b>1.1</b>	<b>0.92</b>	<b>0.87</b>

- For SiC system, **LiPb** provides highest breeding among ALL breeders
- Overall TBR of thick LiSn/SiC and FLiBe/SiC blankets will not exceed 1.0
- Need to use Be with LiSn/SiC and FLiBe/SiC blankets to achieve TBR of 1.1
- **Main features of LiPb/SiC Blanket:**
  - 5 cm thick FW (40% SiC, 60% LiPb)
  - 25 cm thick IB blanket (8% SiC, 92% LiPb)
  - 55 cm thick OB blanket (8% SiC, 92% LiPb)
  - 90% enriched Li<sup>6</sup>
- **3-D results for LiPb/SiC blanket:**

<b>Overall TBR</b>	<b>1.1</b>
<b>Overall Mn</b>	<b>1.1</b>
- **Energy recovered from all components except water-cooled LT shield**

## Partial Cross Section of Outboard Blanket



## Cross Section of ARIES-ST Blanket



# Shielding Requirements



- Provide lifetime protection for **S/C magnets**  $< 10^{19}$  n/cm<sup>2</sup>
- Provide lifetime protection for **V.V.**  $< 1$  He appm
- Protect **workers/personnel**  $< 2.5$  mRem/h
- **Power production** component  
( $< 1\%$  nuclear heating in LT shield)
- OB shield is **lifetime component**  $< 200$  dpa for FS  
 $< 3\%$  burnup for SiC
- Reasonable **cost**
- Attractive **safety** & environmental characteristics:
  - Compatible with FPC components
  - Low level waste (Class C)
  - No hazardous materials
  - No damage in case of LOCA/LOFA
- **Clear** as many components as design allows for reasonable cost
- Meet stress and temperature limits
- Reliable, maintainable, replaceable, recyclable

# Inboard Shielding Options for ARIES-ST



- Candidate materials:

<u>Structure</u>	<u>Coolant**</u>	<u>Filler</u>
FS	He	FS
	H <sub>2</sub> O	W
	D <sub>2</sub> O	WC
	LiPb	WB
- W-based shields are not attractive options:
  - generates high decay heat
  - degrades outboard breeding

- Features of candidate inboard shields:

## I- Helium cooled FS FW/shield:

- + 20 cm thick shield
- + 400 MW i/b heating recovered
- + high Mn (1.1)
- + acceptable outboard breeding for FS/He shield only
- + safety barrier between CP and blanket
- 25 MW higher Joule losses in CP
- 40 MW<sub>e</sub> He pumping power (~90% recovered as thermal heat)

## II- Water cooled FS FW/shield:

- + 12 cm thick shield
- + 25 MW lower Joule losses in CP
- **marginal** outboard breeding
- 400 MW i/b heating dumped as low grade heat
- low Mn (1.0)
- water radiolysis and corrosion problems
- need T removal system for water loop
- larger CP and higher magnet cost

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\*\* 20% He or 10% water in shield

# Conclusions

- Nuclear issues that raised most concern are protection of center post and breeding potential of candidate breeders
- Unshielded CP does not offer an attractive design
- LiPb blanket provides adequate breeding with 5% excess breeding capability
- LiSn and FLiBe will not meet breeding requirements unless Be is used in blanket
- Key neutronics results:

Overall TBR	1.1
Overall $M_n$	1.1
PFC and CP lifetimes	3 FPY
Shield and magnet lifetimes	40 FPY
FW/B EOL Fluence	18 MWy/m <sup>2</sup>
- Good agreement obtained between 1-D and 3-D analyses for global values: overall TBR and  $M_n$
- 1-D analysis overestimates local radiation damage to PFCs and underestimates damage at back of blanket/shield