

# ARIES-AT Radial Build Definition: DCLL Blanket w/ Thin SiC Inserts

# L. El-Guebaly

Fusion Technology Institute UW - Madison

#### **Contributors:**

R. Raffray, S. Malang (UCSD), S. Sharafat, M. Youssef (UCLA)

**ARIES-Pathways Project Meeting** 

January 21 - 22, 2009 UCSD



# Objectives

- Redesign ARIES-AT with DCLL system (a la ARIES-CS) and redefine radial builds with:
  - DCLL blanket and shield
  - < 90% Li enrichment
  - LiPb/He Manifolds (<u>tentative</u> composition/dimension/location)
  - No stabilizing shells (to be added later)
  - LT magnets (instead of HT magnets).
- Assess impact of SiC inserts on TBR:
  - **Reference**: 100% dense, 0.5 cm thick SiC insert
  - Alternative: 0.5-0.7 cm thick Ultramet SiC insert (0.3-0.5 cm 10% dense SiC foam sandwiched between 1 mm 100% dense impermeable CVD-SiC face sheets; 0.23-0.25 cm equivalent SiC thickness).
- Compare reference ARIES-AT with ARIES-AT-DCLL and highlight impact of DCLL system on overall design.



# ARIES-AT Reference Design

Fusion Power 1755 MW

Major Radius 5.2 m Minor Radius 1.3 m

Peak  $\Gamma$  @ IB, OB, Div 3.1, 4.8, 2 MW/m<sup>2</sup>

SiC/SiC Composite Structure

LiPb/SiC Blanket

Discrete LiPb Manifolds

HT S/C Magnet @ 70-80 K

No W on FW

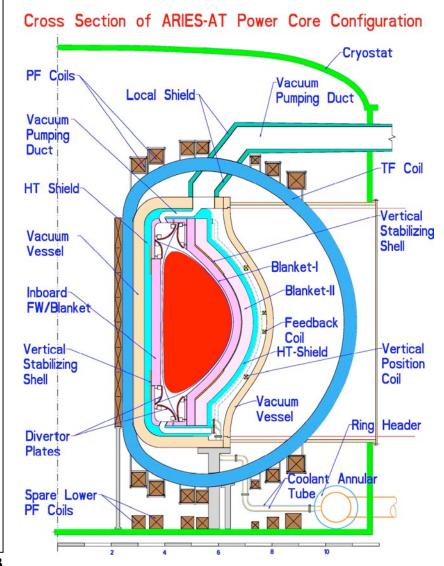
Calculated Overall TBR 1.1

 $\eta_{th}$  ~ 60%

Availability 85%

#### Plasma Control:

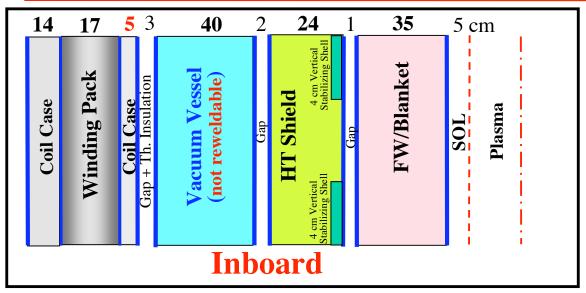
- 5 Tungsten Shells on IB and OB
- 2 Vertical Position Coils
- 2 Feedback Coils

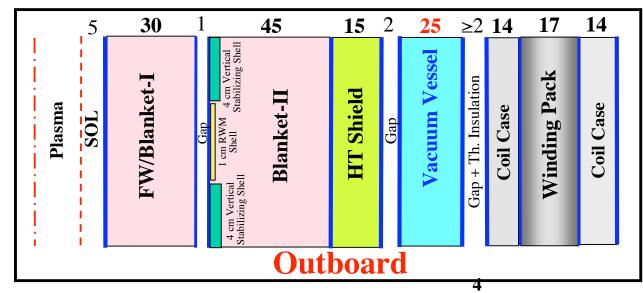


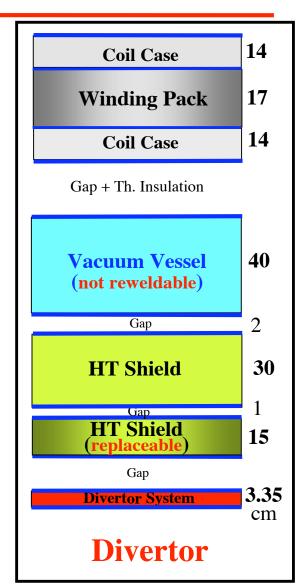


# ARIES-AT Radial Builds: IB, OB, Div

(SiC Structure; HT Magnets)





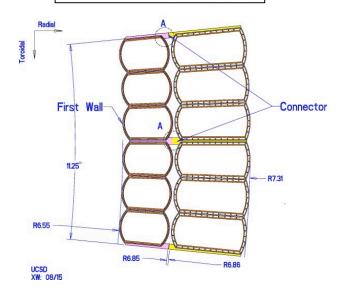




# **ARIES-AT Blanket Options**

# Reference ARIES-AT OB Blanket

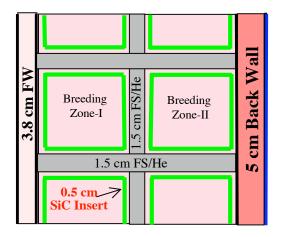
## **SiC Structure**



BreederLiPbCoolantLiPb

# ARIES-AT-DCLL Blanket (a la ARIES-CS)

**FS Structure** 



Breeder LiPbDual Coolants LiPb and He



# **ARIES-AT Compositions**

Inboard:

FW/Blanket

**HT Shield** 

 $\mathbf{V}\mathbf{V}$ 

**Outboard:** 

FW/Blanket-I

FW/Blanket-II

**HT Shield** 

VV Top/Bottom:

**Divertor System** 

Replaceable HT Shield

**Permanent HT Shield** 

 $\mathbf{V}\mathbf{V}$ 

ARIES-AT-LiPb/SiC (Reference Design)

81% LiPb, 19%SiC

15%SiC, 10% LiPb, 70% B-FS Filler, **5% W shells** 13% FS, 22% H<sub>2</sub>O, 65% WC

80% LiPb, 20%SiC

77% LiPb, 20%SiC, **3% W shells** 

15%SiC, 10% LiPb, 75% B-FS Filler 30% FS, 70% H<sub>2</sub>O

40%SiC, 50% LiPb, 10% W

15%SiC, 10% LiPb, 75% FS Filler

15%SiC, 10% LiPb, 75% B-FS Filler 13% FS, 22% H<sub>2</sub>O, 65% WC ARIES-AT-DCLL
0.5 cm Ultramet, No Shells

79% LiPb, 12% He/void, 6% FS, 3%SiC inserts 15%FS, 10% He, 75% B-FS Filler 17% FS, 34% H<sub>2</sub>O, 49% WC

79% LiPb, 12% He/void, 6% FS, 3%SiC inserts

---

15%FS, 10% He, 75% B-FS Filler 30% FS, 50% H<sub>2</sub>O, 20% B-FS

33% FS, 4% W, 63% He

15%FS, 10% He, 75% B-FS Filler

15%FS, 10% He, 75% B-FS Filler 22% FS, 48% H<sub>2</sub>O, 30% B-FS



# ARIES-AT-DCLL Radiation Limits and Key Parameters

Calculated Overall TBR	1.1	
Net TBR (for T self-sufficiency)	~1.01	
Damage to Structure (for structural integrity)	200	dpa - advanced FS
Helium Production @ VV (for reweldability of FS)	1	He appm
HT S/C TF & PF Magnets (@ 70-80 K):  Peak Fast n fluence to Nb <sub>3</sub> Sn (E <sub>n</sub> > 0.1 MeV)  Peak Nuclear heating  Peak dpa to Cu stabilizer  Peak Dose to GFF Polyimide insulator	$   \begin{array}{r}     10^{19} \\     2 \\     6x10^{-3} \\     < 10^{11}   \end{array} $	n/cm <sup>2</sup> mW/cm <sup>3</sup> dpa rads
Plant Lifetime	40	FPY
Availability	85%	
<b>Operational Dose to Workers and Public</b>	< 2.5	mrem/h



# Changes and Updates

ARIES-AT-LiPb/SiC

ORNL FS

Li enrichment Average temp Density

Peak NWL @ IB, OB, Div

**SiC** inserts

**FS** structure

LiPb:

**OB** blanket

**Shells:** 

Two VS shells on IB: (toroidally continuous) Two VS shells on OB: (toroidally continuous)

**RWM** shell on **OB**:

**Breeder/coolant manifolds** 

**Shield coolant** 

IB Blanket-shield gap

VV model

**Magnets** 

**Cross section data library** 

(Reference Design)

 $3.1, 4.8, 2 \text{ MW/m}^2$ 

90% 700 °C 8.8 g/cc

Two segments

4 cm W between IB blanket & shield

4 cm W between OB blanket segments

1 cm W between OB blanket segments

Discrete

LiPb

1 cm

Homogeneous

HT YBCO

IAEA FENDL-2

**ARIES-AT-DCLL** 

3.4, 4.8, 2 MW/m<sup>2</sup> (to be confirmed with 3-D)

MF82H FS

< 90% 580 °C 9 g/cc

0.5 cm thick Ultramet

One or two segments?

Cu shell between IB blanket & shield

Cu shell behind OB blanket or between OB blanket segments?

0.5 cm Cu shell behind OB FW or between OB blanket segments?

Toroidally continuous: 25 cm He/LiPb manifolds for IB blanket & shield 35 cm He/LiPb manifolds for OB blanket & shield 20 cm He manifolds for divertor shield (to be confirmed)

He

Heterogeneous with 2-cm-thick plates

LT Nb<sub>3</sub>Sn (a la ARIES-RS)

IAEA FENDL-2.1



# Ultramet SiC Inserts

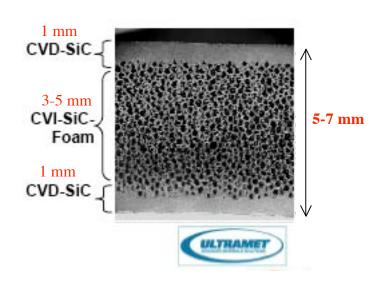
(Ref: S. Sharafat, Development Status of Flow Channel Inserts for the U.S.-ITER DCLL TBM; 18th TOFE, 2008)

#### Main features and advantages:

- 3-5 mm 10% dense foam
- Fully dense CVD SiC face sheets prevent LiPb ingress into foam
- Low SiC content (to alleviate impact on tritium breeding)
- Construction of long segments (> 75 cm) seems feasible
- Low-cost manufacturability
- Good strength, stiffness, and thermal stress resistance
- Low thermal and electrical conductivity.

Testing is underway.

Results so far are promising.

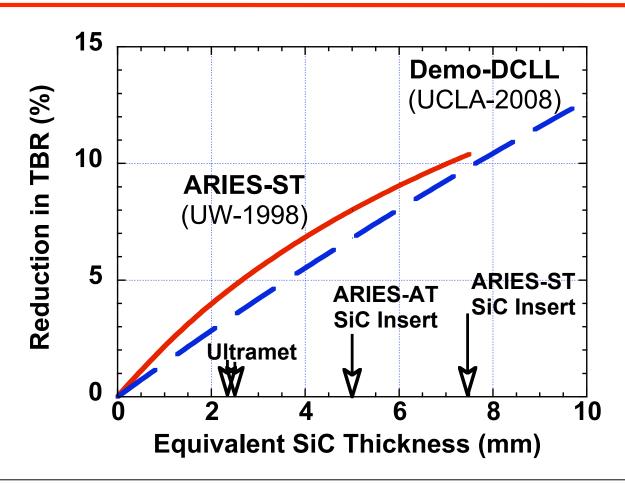


### For any type of SiC inserts:

Change of electric conductivity with neutron irradiation could be significant (0.4 at% Mg @ 3 FPY, per Sawan (UW)).



# SiC Inserts Degrade Tritium Breeding

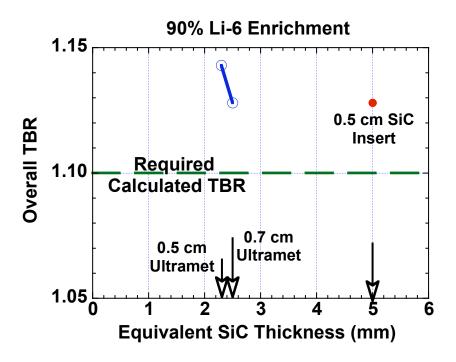


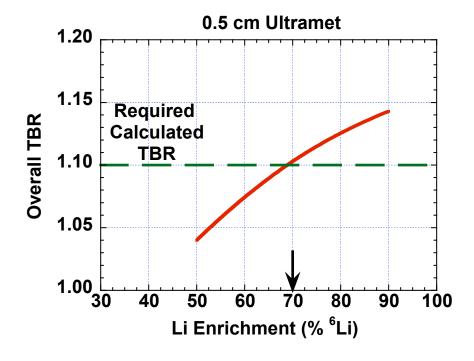
Ultramet alleviate impact of SiC on TBR, allowing lower enrichment (< 90%) and/or thinner blanket



# ARIES-AT-DCLL TBR

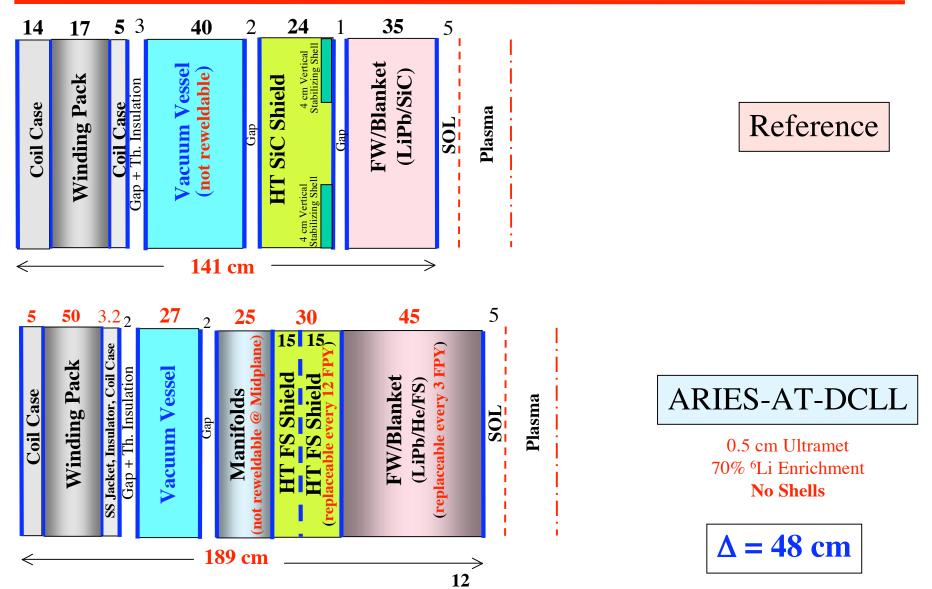
45 cm IB FW/Blanket/Back Wall 80 cm OB FW/Blanket/Back Wall No Shells





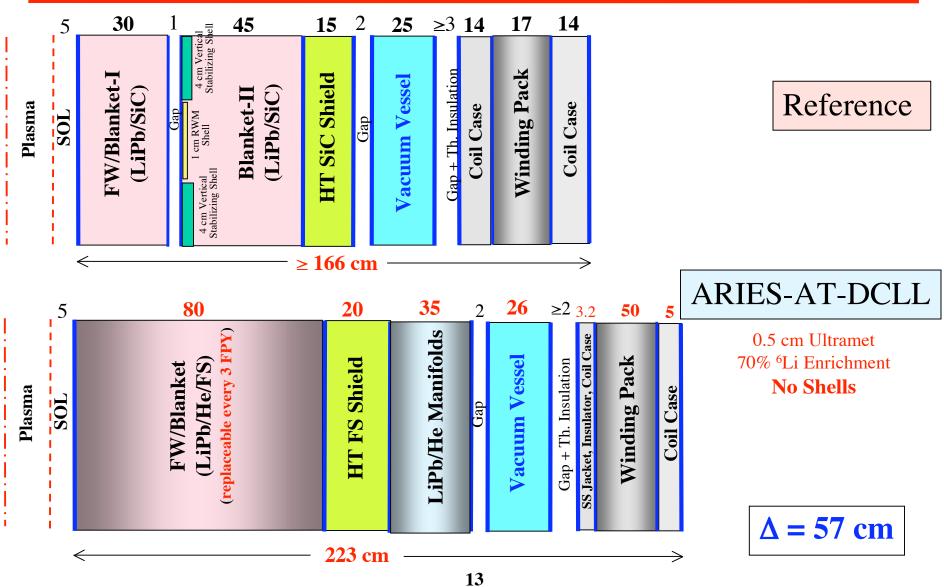


# ARIES-AT IB Radial Build



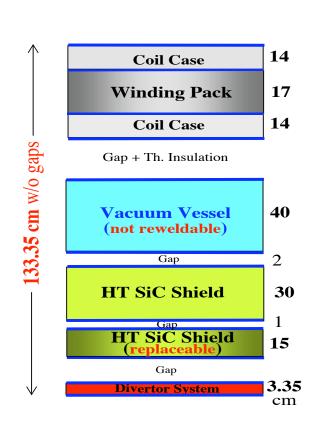


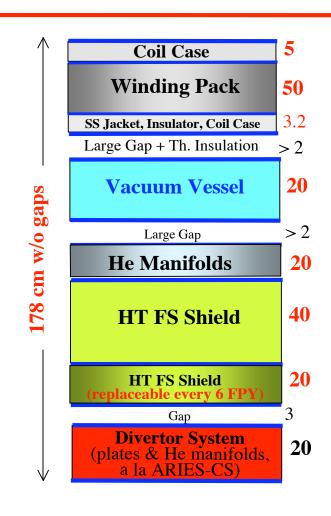
# ARIES-AT OB Radial Build





## **ARIES-AT Divertor Radial Build**





 $\Delta = 45 \text{ cm}$ 

Reference

**ARIES-AT-DCLL** 



# **Radiation Level**

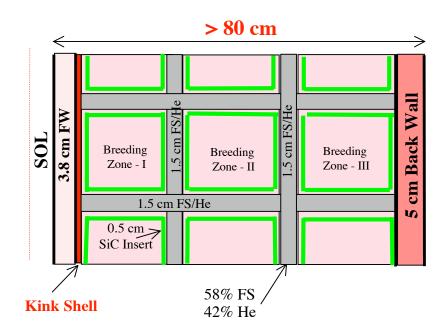
	IB	OB	Div.	Limit
Peak NWL (MW/m <sup>2</sup> )	3.4	4.8	2	
dpa at shield (dpa @ 40 FPY): Replaceable Permanent	640 160	 109	1 <mark>080</mark> 160	200
He production at manifolds (He appm @ 40 FPY)	<b>5</b> *	1	0.8	1
He production at VV (He appm @ 40 FPY)	1	0.2	0.1	1
HT Magnet @ 4 K: Fast neutron fluence (10 <sup>19</sup> n/cm <sup>2</sup> @ 40 FPY)	1	0.5	0.7	1
Nuclear <b>heating</b> (mW/cm <sup>3</sup> )	0.6	2	1	2

<sup>\*</sup> Rewelding allowed at top/bottom, not around midplane.

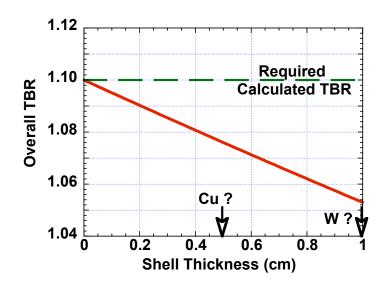


### Kink Shell Behind OB FW?

- Could Cu (or W) kink shell be placed behind OB FW?
- Integration of kink shell with blanket?
- Impact on breeding?



ARIES-AT-DCLL OB Blanket with kink shell behind FW



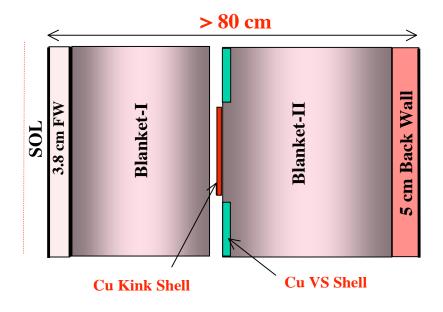
IB and/or OB Blanket should be thickened to compensate for losses in breeding



# Shells Between OB Blanket Segments?

- Could OB blanket be segmented into two segments?
- Advantages:
  - Less integration problems
  - Less impact of shells on breeding
  - Lifetime of back segment > 3 FPY ( $\sim 15$  FPY)
  - Notable reduction in lifecycle radwaste volume.

ARIES-AT-DCLL OB Blanket with Cu kink and VS shells between OB blanket segments (blanket temp < 700 °C)





# Impact of DCLL System on ARIES-AT Economics

	ARIES-AT-LiPb/SiC (Reference)	ARIES-AT-DCLL	Cost of ARIES-AT-DCLL
IB, OB, Div radial standoff*	<b>135</b> , 160, 133	<b>185</b> , 219, 178	<b>↑</b>
Major radius	5.2 m	> 5.2 m	<b>↑</b>
Calculated overall <b>TBR</b>	1.1	1.1 w/o shells	
FW/blanket lifetime	4 FPY	2.8 FPY	<b>↑</b>
Overall energy multiplication	1.1	~1.15	$\downarrow$
Structure unit cost (2004 \$)	510 \$/kg	103 \$/kg	$\downarrow$
$\eta_{th}$	~ 60%	40-45%	<b>↑</b>
Cost of <b>heat transfer/transport system</b> (1992 \$)	\$126M	>\$300M	<b>↑</b>
He pumping power		$> 100 \text{ MW}_{e}$	<b>↑</b>
Level of Safety Assurance (LSA) factor	1	2	<b>↑</b>
COE:			<b>↑</b>
in 1992 \$	48 mills/kWh	> 60 mills/kWh	
in 2004 \$	60 mills/kWh	> 80 mills/kWh	

<sup>\*</sup> Excluding gaps.



## Observations and Needed Info

#### **Observations:**

- DCLL system increases radial standoff ⇒ Larger and costly machine
- 0.5 cm Ultramet has less impact on breeding compared to 0.5 cm SiC inserts
- IB manifolds are not reweldable near midplane.
- Adding stabilizing shells will degrade breeding, requiring thicker IB/OB blankets
- Segmenting OB blanket offers design advantages.

#### **Needed info:**

- Locations of kink shells, vertical stabilizing shells, and feedback coils
- One or two OB blanket segments?
- Confirm manifolds size, composition, and location.

#### To be considered:

- Change of SiC electric conductivity with neutron irradiation
- Change of electric conductivity of stabilizing shells with neutron irradiation